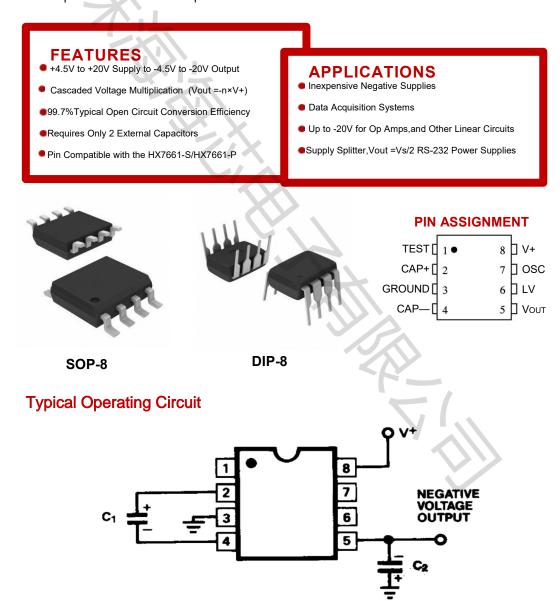
HX7661-S/HX7661-P CMOS Voltage Converters

The HX7661-S/HX7661-P is a monolithic charge pump voltage inverter designed to convert a positive voltage in the range of +4.5V to +20V into the corresponding negative voltage of -4.5V to -20V. Compared to previous implementations of charge pump voltage inverters, the HX7661-S/HX7661-P offers superior performance by combining low quiescent current with high efficiency. It integrates an oscillator, control circuitry, and 4 power MOS switches on-chip, requiring only two low-cost capacitors as external components.



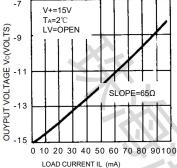
Symbol	Limit	Unit
V+TO GND	-0.3.+22	V
Oscillator Input to GND(Note 1)		
V-<12V	-0.3 V++0.3	V
V+>12V	V+-12.3.V++0.3V	V
Power Dissipation (Note 2)		
Plastic DIP	300	mW
SO	500	mW
TO-99	500	mW
CERDIP	500	mW
Operating Temperature Ranges		
Commercial	0 to +70	$^{\circ}$
Extended	-40 to +85	$^{\circ}$
Military	-55 to +125	$^{\circ}$
Storage Temperature	-65 to +160	$^{\circ}$
ad Temperature	+300	$^{\circ}\mathbb{C}$

ELECTRICAL CHA	RACTE	RISTICS						
PARAMETER	SYMBOL	CONDITIONS		MIN	TYP	MAX	UNITS	
Supply Voltage Range-Lo	V+L	RL=10k2,LV=GND	55℃ <ta<+125℃< td=""><td>4.5</td><td></td><td>11</td><td></td></ta<+125℃<>	4.5		11		
Supply Voltage Range-Hi	V+H RI	RL=10k2,LV=Open	40℃ <t <+85℃<="" td=""><td>9</td><td></td><td>20</td><td>V</td></t>	9		20	V	
Ouppry Voltage Hange-III	V	TC-TOKZ,EV-Open	55℃< +125℃	9		16.5		
			TA=+25℃		0.25	0.60		
Supply Current	l+	RL=o,LV=Open	0°C <ta<+70°c< td=""><td></td><td>0.30</td><td>0.85</td><td rowspan="2">mA</td></ta<+70°c<>		0.30	0.85	mA	
			55℃ <ta<+125c< td=""><td></td><td>0.40</td><td>1.0</td></ta<+125c<>		0.40	1.0		
			TA=+25℃	l.	60	100	Ω	
Output Source Resistance	Ro	lo =20mA,LV =Open	0°C <ta<+70°c< td=""><td></td><td>70</td><td>120</td></ta<+70°c<>		70	120		
			55°℃ <ta<+125℃< td=""><td></td><td>90</td><td>150</td></ta<+125℃<>		90	150		
	I+	V+=5V, RL=00,LV=GND	TA=+25℃		20	150	μΑ	
Supply Current			0℃ <ta<+70℃< td=""><td></td><td>25</td><td>200</td></ta<+70℃<>		25	200		
			-55℃ <ta<+125c< td=""><td></td><td>30</td><td>250</td><td></td></ta<+125c<>		30	250		
	Ro	V+=5V, lo =3mA, LV =GND	TA=+25℃		125	200	Ω	
Output Source Resistance			0°C <ta<+70°c< td=""><td></td><td>150</td><td>250</td></ta<+70°c<>		150	250		
			-55℃ <ta<+125℃< td=""><td></td><td>200</td><td>350</td><td colspan="2"></td></ta<+125℃<>		200	350		
Oscillator Frequency	fosc				10		kHz	
Power Efficiency	Peff	RL=2kQ	TA=+25℃	93	96		<u></u> %	
			Min <ta<max< td=""><td>90</td><td>95</td><td></td><td colspan="2">,,,</td></ta<max<>	90	95		,,,	
Voltage Conversion	VoEf	RL=∞	Min <ta<max< td=""><td>97</td><td>99.9</td><td></td><td>%</td></ta<max<>	97	99.9		%	
Oscillator Sink or Source	losc	V+=5V(Vosc	=OV to +5V)		0.5		μA	
Current	1000	V+=15V(Vosc=+5V to+15V)			4.0		μΑ	

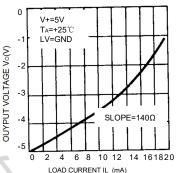
Notes

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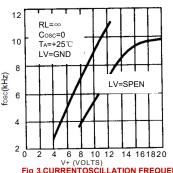
a. Connecting any terminal to voltages greater than V+or less than ground may cause destructive latchup.It is recommended that no input from sources operating from external supplies be applied prior to power-up of the HX7661-S/HX7661-P.
b. Derate linearly above +50°C by 5.5mW/°C c.Pin 1 is a test pin and is not connected in normal use.



LOAD CURRENT IL (mA)
Fig 1. OUTPUT VOLTAGE VS.LOAD CURRENT

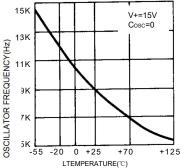


LOAD CURRENT IL (mA)
Fig 2. OUTPUT VOLTAGE VS.LOAD CURRENT

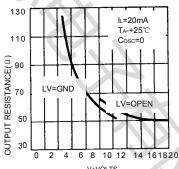


V+ (VOLTS)

Fig 3.CURRENTOSCILLATION FREQUENCY
Vs.SUPPLY VOLTAGE



4. UNOADED OSCILLATOR FREQUENCY vs. TEMPERATURE



V+VOLTS
Fig 5. OUTPUT SOURCE RESLSTANCE vs.
SUPPLY VOLTAGE

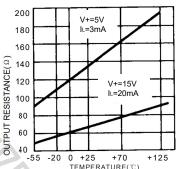


Fig 6.CURRENTO SPURCE RESISTANCE vs. TEMPERATURE

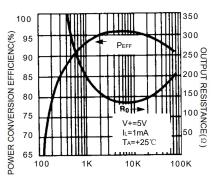
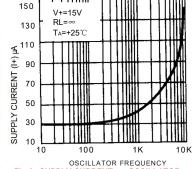
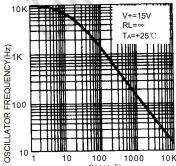


Fig 7 . POWER CONVERSION FREQUENCY AND OUTPUT RESISTANCE vs. OSCILLATOR FREQUENCY



OSCILLATOR FREQUENCY
Fig 8. SUPPLY CURRENT vs. OSCILLATOR
FREQUENCY



Cosc(pF)
Fig 9.OSCILLATION FREQUENCY vs. EXTERNAL OSCILLATOR CAPACITANCE

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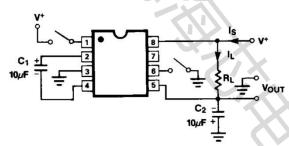
www.haixindianzi.com Detailed Description

The HX7661-S/HX7661-P is a fully integrated circuit that incorporates all the necessary components to function as a voltage inverter. It requires only two external capacitors, typically inexpensive 10uF polarized electrolytic capacitors. Figure 2 illustrates the operation of the HX7661-S/HX7661-P as an idealized voltage inverter.

In the first half of the cycle, switches S2 and S4 are kept open, while switches S1 and S3 are closed. This allows the capacitor C1 to charge to a voltage equal to Vin. Then, in the second half of the cycle, switches S1 and S3 are opened, and switches S2 and S4 are closed. As a result, the capacitor C1 undergoes a negative shift, equivalent to Vin.

Assuming ideal switches (with zero resistance, Ron = 0) and no load on C2, the charge from C1 is then transferred to C2. This transfer ensures that the voltage on C2 is precisely the negative of Vin, i.e., -Vin.

The four switches depicted in Figure 2 are MOS power switches. Specifically, switch S1 is a P-channel switch, while switches S2, S3, and S4 are N-channel devices.



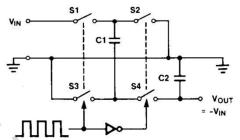


Figure 1.HX7661-S/HX7661-S Test Circuit

Figure 2.Idealized Negative Voltage Converter

Efficiency Considerations

In theory, a voltage multiplier can achieve nearly 100% efficiency provided certain conditions are satisfied. The HX7661-S/HX7661-P approximates the conditions necessary for efficient negative voltage multiplication when large-valued capacitors C1 and C2 are employed. These conditions include:

- The output switches exhibit virtually no offset voltage and have extremely low ON resistance.
- The power consumed by the drive circuitry is minimal.
- The impedances of the reservoir capacitor (C1) and the pump capacitor (C2) are negligible.

The energy loss per charge pump cycle can be expressed as:

$$E = k \times C1 \times (Vin^2 - Vout^2)$$

There will be a significant voltage drop between Vin and Vout if the impedances of C1 and C2 (at the pump frequency) are comparatively high with respect to the output load R1. To minimize output ripple, it is practical to use a large value for C2. Furthermore, increasing the values of both C1 and C2 will enhance the overall efficiency of the voltage multiplier.

General Precautions

Here is a reorganized version of the text with the same meaning:

The positive terminal of capacitor C1 must be connected to Pin 2 of the HX7661-S/HX7661-P, while the positive terminal of capacitor C2 should be grounded.

Always ensure not to exceed the maximum specified supply voltages.

For improved efficiency, when using supply voltages less than 8 volts, connect the LV pin to Ground.

Avoid shorting Vout to V+ for extended periods of time. However, transient conditions, including during startup, are acceptable.

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Applications

Changing Oscillator Frequency

Normally, the OSC pin of the HX7661-S/HX7661-P is left open, utilizing the nominal frequency of 10kHz (or a charge pump frequency of 5kHz). However, to lower the oscillator frequency, an external capacitor can be connected between the OSC and V+ pins (see Figure 3). A graph in the "Typical Operating Characteristics" section illustrates the relationship between the nominal frequency and the capacitor value. Reducing the oscillator frequency will enhance conversion efficiency when dealing with very low output current values. Nevertheless, a drawback of lowering the oscillator frequency is an increase in the impedance level of the pump capacitor. To compensate for this effect, the values of C1 and C2 can be increased.

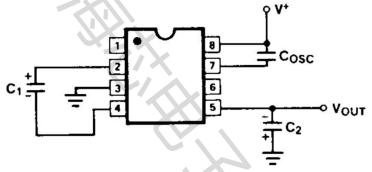


Figure 3.Lowering Oscillator Frequency

In certain applications, especially audio amplifiers, the 5kHz output ripple frequency can be undesirable. There are two methods to increase the oscillator frequency. The first approach is to overdrive the OSC pin using an external oscillator. To prevent the risk of latchup, it is recommended to insert a $1k\Omega$ resistor in series with the OSC input (see Figure 4). If the external clock source does not pull up close to V+, then a $10k\Omega$ pullup resistor is advisable. With this configuration, the pump frequency, and consequently, the output ripple, will be half of the external clock frequency. While driving the HX7661-S/HX7661-P with a higher frequency clock will slightly increase the supply current, it enables the use of smaller external capacitors and raises the ripple frequency.

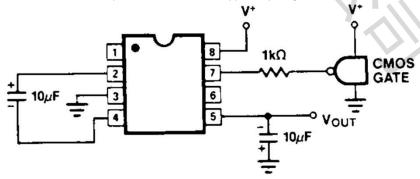


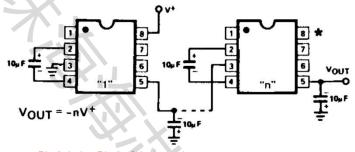
Figure 4.External Clocking

The second approach is to connect pin 1 (TEST) to V+. This effectively disconnects the internal oscillator from the OSC pin. Since there is always a minimal amount of parasitic capacitance present at the OSC pin, connecting the TEST pin to V+ allows the capacitor to oscillate at a faster rate, depending on the amount of parasitic capacitance originating from the OSC pin.

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Cascading Devices

To achieve a larger negative voltage multiplication factor from the initial supply voltage, the HX7661-S/HX7661-P can be cascaded in a configuration as depicted in Figure 5. The resulting output resistance is approximately equivalent to the weighted sum of the individual HX7661-S/HX7661-P Rout values. For lighter loads, the practical limitation is up to 10 devices. The output voltage is defined by the formula Vout = $-n \times V+$ (where n is an integer representing the number of cascaded devices).



Pin 8 tied to Pin 3 of device n-1.

Figure 5. Cascading HX7661-S/HX7661-P for Increased Output Voltage

Negative Voltage Converter

The HX7661-S/HX7661-P is primarily utilized as a charge pump voltage inverter, effectively transforming a positive voltage into its corresponding negative equivalent. As depicted in the simplified circuit of Figure 6, it requires only two external components, namely C1 and C2, typically low-cost 10uF electrolytic capacitors. It is important to note that the HX7661-S/HX7661-P is not a voltage regulator. When powered by a +15V supply, its output source resistance approximates 60Ω . This signifies that, under light loads (less than 1mA load current), the output voltage will be -15V. However, with an increased load current of 10mA, the output voltage will slightly drop to -14.4V. The total output source impedance of the entire circuit is a combination of the HX7661-S/HX7661-P 's output resistance and the impedance of the pump capacitor at the pumping frequency.

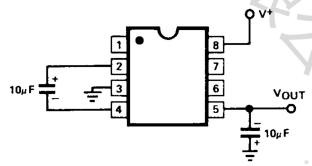


Figure 6.Negative Voltage Converter

The output ripple of the voltage inverter can be calcu-lated by noting that the output current is supplied solely by the reservoir capacitor during one-half of the charge pump cycle. This introduces an output ripple of:

VRIPPLE=k×lour×(1/FpuMP)×(1/C2)

For the nominal Fpump of 5kHz(one-half of the nom-inal 10kHz oscillator frequency)and a 10µF C2,theoutput ripple will be approximately 10mV with a loadcurrent of 10mA.

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ZHHXDZ 珠海海芯电子有限公司

www.haixindianzi.com Positive Voltage Doubler

The HX7661-S/HX7661-P can double a positive voltage asshown in Figure 7.It basically uses the HX7661-S/HX7661-P as a power inverter. The only drawback from this circuit is the inevitable voltage drop across the two diodes.

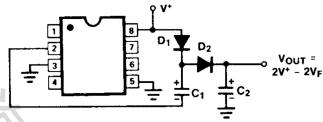
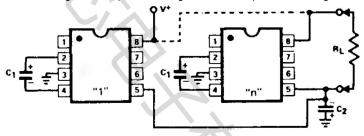


Figure 7.Positive Voltage Doubler

Paralleling Devices

Connecting multiple HX7661-S/HX7661-P in parallel effectively reduces the overall output resistance. As depicted in Figure 8, each individual device requires its own dedicated pump capacitor, labeled C1. However, the reservoir capacitor, denoted as 'C2', serves as a shared component for all paralleled devices. The equation for calculating the reduced output resistance resulting from this parallel configuration is also presented in Figure 8.



 $R_{OUT} = \frac{R_{OUT}(of HX7661-S/HX7661-P)}{n(number of devices)}$

Figure 8.Paralleling HX7661-S/HX7661-Ps to Reduce Output Resistance

Combining Positive Voltage Multiplication and Negative Voltage Conversion

Figure 9 demonstrates the dual functionality of combining positive voltage multiplication and negative voltage conversion. In this circuit, capacitors C1 and C3 serve as the pump and reservoir capacitors respectively for generating the negative voltage. Meanwhile, capacitors C2 (pump capacitor) and C4 (reservoir capacitor) are utilized for the positive voltage converter. However, this circuit configuration leads to a higher source impedance of the generated power supplies, primarily due to the finite impedance of the shared charge pump driver.

Voltage Splitting

The HX7661-S/HX7661-P can also be employed to split a power supply or battery. As shown in Figure 10, the positive terminal of the power supply is connected to V+, while the negative terminal is connected to Vout. The midpoint of the power supply is found on Pin 3. This configuration offers a significantly lower output resistance compared to other applications, enabling higher currents to be drawn from it.

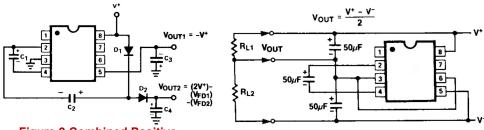


Figure 9.Combined Positive

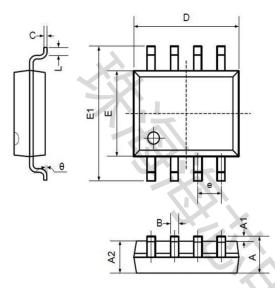
Multiplier and NegativeConverter

Figure 10.Splitting a Supply in Half

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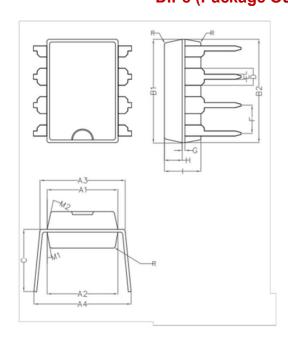
Package Information





Symbol	2.07 (73.00.00)	nsions meters	Dimensions In Inches		
	Min	Max	Min	Max	
Α	1.350	1.750	0.053	0.069	
A1	0.100	0.250	0.004	0.010	
A2	1.350	1.550	0.053	0.061	
В	0.330	0.510	0.013	0.020	
С	0.190	0.250	0.007	0.010	
D	4.780	5.000	0.188	0.197	
E	3.800	4.000	0.150	0.157	
E1	5.800	6.300	0.228	0.248	
е	1.270TYP		0.050TYP		
L	0.400	1.270	0.016	0.050	
θ	0°	8°	0°	8°	

DIP8 (Package Outline Dimensions)



Symbol	Min	Non	Max	
A1	6.28	6.33	6.38	
A2	6.33	6.38	6.43	
A3	7.52	7.62	7.72	
A4	7.80	8.40	9.00	
B1	9.15	9.20	9.25	
B2	9.20	9.25	9.30	
С		5.57		
D		1.52		
E	0.43	0.45	0.47	
F		2.54		
G		0.25		
Н	1.54	1.59	1.64	
1	3.22	3.27	3.32	
R		0.20		
M1	9°	10°	11°	
M2	11°	12°	13°	

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