



MP2980

36V, Synchronous Buck-Boost Controller with Digital Interface and Current Monitor

DESCRIPTION

The MP2980 is a synchronous, four-switch, buck-boost controller capable of regulating different output voltages with a wide input voltage (V_{IN}) range and high efficiency. The MP2980 provides a digital interface that supports output voltage (V_{OUT}) configuration, V_{OUT} slew-rate control, and constant output current (I_{OUT}) limit configuration. This makes the MP2980 well-suited for USB power delivery (PD) designs in USB Type-C power supplies.

The MP2980 uses valley current control in buck mode and peak current control in boost mode to provide fast load transient response and smooth buck-boost mode transients. The MP2980 provides forced continuous conduction mode (FCCM) and a configurable average current limit, which support flexible designs for different applications.

The MP2980 also provides configurable over-current protection (OCP), over-voltage protection (OVP), and V_{IN} under-voltage lockout (UVLO) hysteresis.

The MP2980 is available in a QFN-32 (4mmx4mm) package.

FEATURES

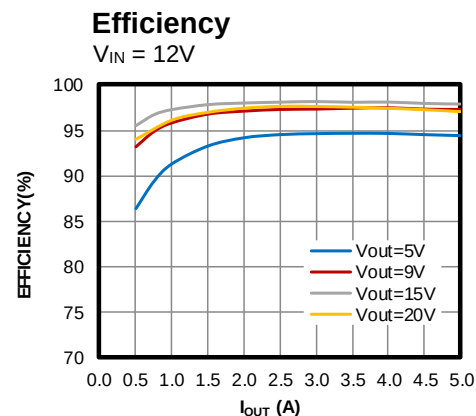
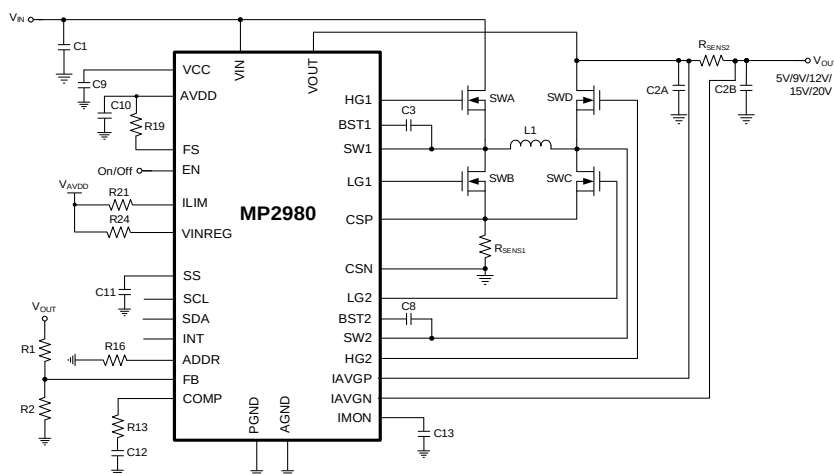
- 6V to 36V Start-Up Input Voltage (V_{IN}) Range
- 5V to 36V Operating V_{IN} Range
- Flexible Digital Interface Control:
 - 0.5V to 28V Output Voltage (V_{OUT}) Range
 - 0.3V to 2.047V Reference Voltage (V_{REF}) Range with 1mV Step
- Selectable V_{OUT} Slew Rate
- Configurable Constant Current Limit
- Output Current (I_{OUT}) Monitor Function (IMON)
- Configurable Soft-Start Time (t_{SS})
- Switching Frequency Spread Spectrum (FSS) for EMI Optimization
- Integrated V_{OUT} Discharge Function
- Selectable 200kHz, 300kHz, 400kHz, and 600kHz Switching Frequency (f_{SW})
- Forced Continuous Conduction Mode (FCCM)
- Configurable V_{IN} Under-Voltage Lockout (UVLO) Hysteresis
- Minimum V_{IN} Regulation
- Over-Current Protection (OCP), Short-Circuit Protection (SCP), and Over-Voltage Protection (OVP)
- Interrupt Indicator for OCP, OVP, and V_{OUT} Power Not Good (PNG)
- Available in a QFN-32 (4mmx4mm) Package

APPLICATIONS

- USB Power Delivery (PD)
- Industrial PC Power Supplies
- Supercapacitor Charging

All MPS parts are lead-free, halogen-free, and adhere to the RoHS directive. For MPS green status, please visit the MPS website under Quality Assurance. "MPS", the MPS logo, and "Simple, Easy Solutions" are registered trademarks of Monolithic Power Systems, Inc. or its subsidiaries.

TYPICAL APPLICATION



ORDERING INFORMATION

Part Number*	Package	Top Marking	MSL Rating
MP2980GR	QFN-32 (4mmx4mm)	See Below	1
EVKT-MP2980	Evaluation kit	N/A	N/A

* For Tape & Reel, add suffix -Z (e.g. MP2980GR-Z).

TOP MARKING

MPSYWW

MP2980

LLLLLL

MPS: MPS prefix
Y: Year code
WW: Week code
MP2980: Part number
LLLLLL: Lot number

EVKT-MP2980 EVALUATION KIT

EVKT-MP2980 kit contents (items below can be ordered separately).

#	Part Number	Item	Quantity
1	EV2980-R-00A	MP2980GR evaluation board	1
2	EVKT-USBI2C-02 bag	Includes one USB to digital communication interface device, one USB cable, and one ribbon cable	1

Order directly from [MonolithicPower.com](https://www.MonolithicPower.com) or our distributors.

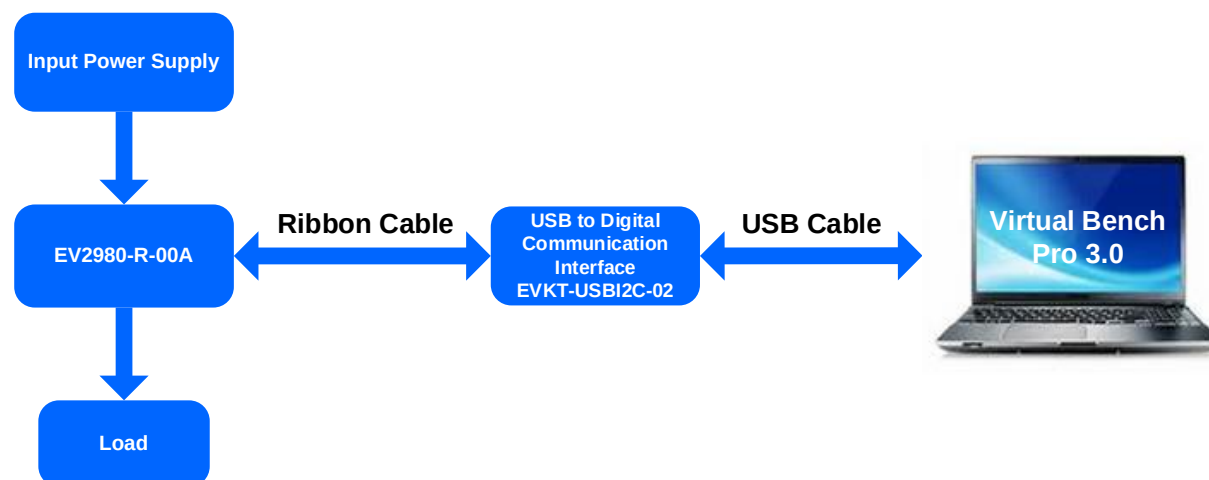
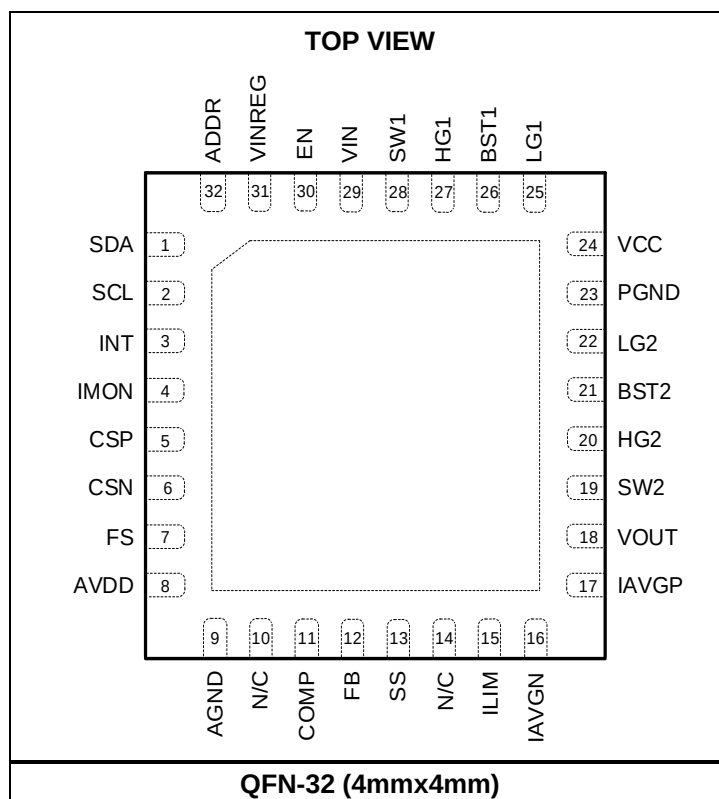


Figure 1: EVKT-MP2980 Evaluation Kit Set-Up

PACKAGE REFERENCE



PIN FUNCTIONS

Pin #	Name	Description
1	SDA	Digital interface data signal.
2	SCL	Digital interface clock signal.
3	INT	Interrupt for power not good (PNG), over-current protection (OCP), over-temperature protection (OTP), and over-voltage protection (OVP) events. In the default set-up, the INT pin is masked off in response to a PNG event. INT is an open-drain output and is pulled low if an interrupt event occurs. Once the fault is removed, INT recovers to open drain. INT is also an open drain when the IC is not enabled.
4	IMON	Current monitor output. The IMON pin indicates the signal between the IAVGP and IAVGN pins.
5	CSP	Positive input of the switching current-sense signal. Connect the CSP pin to the high side of the current-sense resistor.
6	CSN	Negative input of the switching current-sense signal. Connect the CSN pin to the low side of the current-sense resistor.
7	FS	Register bits FSW[7:6] default value configuration. The FS pin provides two different voltage levels during start-up to set the default FS voltage (V_{FS}): V_{FS1} : $0.51 \times AVDD$ to $0.68 \times AVDD$, FSW = 00 (200kHz) V_{FS2} : $0.74 \times AVDD$ or above, FSW = 10 (400kHz) FS cannot be floated or connected to ground. See the Electrical Characteristics section on page 8 for different voltage settings. Changing the voltage level of FS after start-up does not affect register bits FSW[7:6]. These bits can be changed via the digital interface after start-up.
8	AVDD	Internal control circuit bias supply. Decouple the AVDD pin with a $\geq 2.2\mu F$ capacitor.
9	AGND	Analog ground.
10, 14	N/C	No internal connection.
11	COMP	Internal error amplifier output. Connect the COMP pin to a capacitor and a resistor in series with AGND for loop compensation.
12	FB	Output voltage (V_{OUT}) feedback. Connect a resistor divider between the FB and VOUT pins.
13	SS	Soft-start configuration. Connect the SS pin to an external capacitor. SS also sets the off time in hiccup.
15	ILIM	Register bits ILIM[2:0] default value configuration. The ILIM pin provides four different voltage levels during start-up to set the default ILIM voltage (V_{ILIM}): V_{ILIM1} : ILIM = 001 (33.3mV) V_{ILIM2} : ILIM = 011 (45.1mV) V_{ILIM3} : ILIM = 101 (56.8mV) V_{ILIM4} : ILIM = 111 (68.7mV) Float ILIM to set ILIM = 001 by default. See the Electrical Characteristics section on page 8 for different voltage settings. Changing the voltage level of ILIM after start-up does not affect either the register bits ILIM[2:0] or the current limit threshold. These bits can be changed via the digital interface after start-up.
16	IAVGN	Negative terminal of average current limit sense input. The IAVGN pin can only be used to set the output current (I_{OUT}) limit by connecting the pin to the positive terminal of the output rail.
17	IAVGP	Positive terminal of average current limit sense input. The IAVGP pin can only be used to set the I_{OUT} limit by connecting the pin to the positive terminal of the output rail.
18	VOUT	V_{OUT} sense input. The VOUT pin supplies power to VCC based on the VCC power logic. Connect VOUT to the output capacitor (C_{OUT}).

PIN FUNCTIONS *(continued)*

Pin #	Name	Description
19	SW2	Boost switch node of the controller. Connect the SW2 pin to the SWD source and the SWC drain.
20	HG2	Boost high-side MOSFET (HS-FET) gate driver. Connect the HG2 pin directly to the SWD gate.
21	BST2	Bootstrap power for boost HS-FET gate driver. Connect a capacitor between the BST2 and SW2 pins. BST2 is supplied by either VCC or BST1.
22	LG2	Boost low-side MOSFET (LS-FET) gate driver. Connect the LG2 pin directly to the SWC gate.
23	PGND	Power ground. The PGND pin provides the gate-driving current return.
24	VCC	Driver circuit and internal bias supply. Place a $\geq 2.2\mu\text{F}$ decoupling ceramic capacitor as close to the VCC pin as possible. VCC is powered by the input voltage (V_{IN}) or output voltage (V_{OUT}).
25	LG1	Buck LS-FET gate driver. Connect the LG1 pin directly to the SWB gate.
26	BST1	Bootstrap power for buck HS-FET gate driver. Connect a capacitor between the BST1 and SW1 pins. BST1 is supplied by VCC or BST2.
27	HG1	Buck HS-FET gate driver. Connect the HG1 pin directly to the SWA gate.
28	SW1	Buck switch node of the controller. Connect the SW pin to the SWA source and the SWB drain.
29	VIN	Input power supply and voltage sense input.
30	EN	Chip enable control. If not used, connect the EN pin to the input source for automatic start-up. EN can also configure V_{IN} under-voltage lockout (UVLO). Do not float this pin.
31	VINREG	VIN regulation. The VINREG pin sets the minimum operating V_{IN} during switching. If not used, connect VINREG to AVDD.
32	ADDR	Digital interface slave address setting. The ADDR pin sets the default value of the ENPWR bit.

ABSOLUTE MAXIMUM RATINGS ⁽¹⁾

VIN, EN	-0.3V to +40V
VOUT, IAVGP, IAVGN	-0.3V to +30V
VCC	-0.3V to +8.5V
SW1, SW2	
.....	-1V to +40V (-5V to +45V for <20ns)
LG1, LG2	
.....	-0.3V to +10V (-2V to +11V for <20ns)
BST1, HG1	-0.3V to V _{SW1} + 8.5V
BST2, HG2	-0.3V to V _{SW2} + 8.5V
All other pins	0.3V to +6.5V
Continuous power dissipation ^{(2) (5)}	4.4W
Junction temperature (T _J)	150°C
Lead temperature	260°C
Storage temperature	-65°C to +150°C

ESD Ratings ⁽⁴⁾

Human body model (HBM)	±2000V
Charged-device model (CDM)	±2000V

Recommended Operating Conditions ⁽³⁾

Start-up voltage (V _{ST})	6V to 36V
Operating voltage (V _{IN}) ⁽⁵⁾	5V to 36V
Output voltage (V _{OUT})	0.5V to 28V
Operating junction temp (T _J)	-40°C to +125°C

Thermal Resistance

θ_{JA} θ_{JC}

EV2980-R-00A ⁽⁶⁾	28.....8.....°C/W
JESD51-7 ⁽⁷⁾	42.....9.....°C/W

Notes:

- 1) Exceeding these ratings may damage the device.
- 2) The maximum allowable power dissipation is a function of the maximum junction temperature, T_J (MAX), the junction-to-ambient thermal resistance, θ_{JA}, and the ambient temperature, T_A. The maximum allowable continuous power dissipation at any ambient temperature is calculated by P_D (MAX) = (T_J (MAX) - T_A) / θ_{JA}. Exceeding the maximum allowable power dissipation can produce an excessive die temperature, which may cause the regulator to go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- 3) The device is not guaranteed to function outside of its operating conditions.
- 4) HBM, per JEDEC specification JESD22-A114; CDM, per JEDEC specification JESD22-C101, AEC specification AEC-Q100-011. The JEDEC document JEP155 states that 500V HBM allows safe manufacturing with a standard ESD control process. The JEDEC document JEP157 states that 250V CDM allows safe manufacturing with a standard ESD control process. HBM is with regard to ground.
- 5) The operating voltage after V_{OUT} is regulated to a minimum 5V voltage, and the VCC load is below 10mA.
- 6) Measured on the EV2980-R-00A: a 6-layer, 2oz-1oz-1oz-1oz-1oz-2oz PCB (91.4mmx66mm).
- 7) The θ_{JA} value given in this table is only valid for comparison with other packages, and cannot be used for design purposes. These values were calculated in accordance with JESD51-7, and simulated on a specified JEDEC board. They do not represent the performance obtained in an actual application.

ELECTRICAL CHARACTERISTICS

$V_{IN} = 12V$, $V_{OUT} = 12V$, $V_{EN} = 2V$, $T_J = -40^{\circ}C$ to $+125^{\circ}C$ ⁽⁸⁾, typical values are tested at $T_J = 25^{\circ}C$, unless otherwise noted.

Parameter	Symbol	Condition	Min	Typ	Max	Units
Power Supply						
Operating VCC voltage	V _{CC}	V _{IN} = 6V or V _{OUT} = 6V, 0mA to 20mA on VCC	5.1	5.95	6	V
		V _{IN} = 12V or V _{OUT} = 12V, 0mA to 60mA on VCC	6.7	7.2	7.7	V
Input voltage (V _{IN}) under-voltage lockout (UVLO) ⁽⁹⁾	V _{IN_UVLO_R}	V _{IN} rising	5	5.5	5.9	V
V _{CC} UVLO ⁽⁹⁾	V _{CC_UVLO_F}	V _{CC} falling	3.8	4.3	4.8	V
VCC power source change threshold	V _{IN_TH_VCC}	V _{OUT} = 12V, ramp V _{IN} from 5V to 10V	8.1	8.8	9.5	V
	V _{OUT_TH_VCC}	V _{IN} = 12V, ramp V _{OUT} from 5V to 10V	8.1	8.8	9.5	V
AVDD voltage	V _{AVDD}	V _{IN} = 12V, 0mA to 5mA	4.7	5.2	5.6	V
Shutdown current	I _{SD}	V _{EN} = 0V, measured on the VIN and VOUT pins			5	μA
		ENPWR = 0, V _{IN} = 12V, V _{OUT} = 0V, measured on VIN, V _{EN} = 2V	300	510	800	μA
Enable Control (EN Pin)						
EN turn-on threshold	V _{EN_ON}	V _{EN} rising (switching)	1.25	1.35	1.45	V
EN high threshold	V _{EN_H}	V _{EN} rising (micro-power)			1.1	V
EN low threshold	V _{EN_L}	V _{EN} falling (micro-power)	0.4			V
EN turn-on hysteresis current	I _{EN_HYS}	EN > V _{EN_ON} , EN source current	3.2	4.7	6.2	μA
EN input current	I _{EN}	V _{EN} = 0V, 3.3V		0.01		μA
ENPWR turn-on delay ⁽¹⁰⁾	t _{ENPWR_DELAY}	From ENPWR = 1 to switching, C _{SS} = 47nF		1		ms
Feedback (FB) Control						
Reference voltage	V _{REF}	VREF = 7FFH, T _J = 25°C	-1%	2.047	+1%	V
		VREF = 7FFH, T _J = -40°C to +125°C	-2%	2.047	+2%	V
		VREF = 1F4H, T _J = 25°C	-2%	0.5	+2%	V
		VREF = 1F4H, T _J = -40°C to +125°C	-3%	0.5	+3%	V
FB input current	I _{FB}	V _{FB} = 0.52V			200	nA
Error amplifier transconductance	G _{EA}	V _{FB} = V _{REF} + 10mV, V _{COMP} = 2.5V		1220		μA/V
Compensation to current-sense gain ⁽¹⁰⁾	G _{CS}	ΔV _{CS} / ΔV _{COMP}		200		mV/V
SS charge current	I _{CHG_SS}	During soft start and overload recovery	2	6	10	μA
SS discharge current	I _{DSG_SS}	After hiccup protection is triggered		1		μA
VREF change slew rate	t _{REF}	SR = 00	25	38	51	mV/ms
		SR = 11	130	150	170	mV/ms
VINREG reference voltage	V _{VINREG_REF}	T _J = 25°C	1.188	1.2	1.212	V
		T _J = -40°C to +125°C	1.182	1.2	1.218	V
VINREG input current	I _{VINREG}	V _{VINREG} = 1.25V			50	nA

ELECTRICAL CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 12V$, $V_{EN} = 2V$, $T_J = -40^{\circ}C$ to $+125^{\circ}C$ ⁽⁸⁾, typical values are tested at $T_J = 25^{\circ}C$, unless otherwise noted.

Parameter	Symbol	Condition	Min	Typ	Max	Units
Current Limit						
Buck valley current limit	I_{LIMIT_BUCK}		113	133	153	mV
Boost peak current limit	I_{LIMIT_BOOST}		130	150	170	mV
Over-current protection (OCP) hiccup threshold ⁽¹⁰⁾	V_{TH_OCP}			60		% of V_{REF}
Average constant current limit	I_{AV_LIMIT}	$ILIM = 011$, $V_{IAVGN} = 12V$, ramp up V_{IAVGP}	40	45	50	mV
		$ILIM = 111$, $V_{IAVGN} = 12V$, ramp up V_{IAVGP}	62.5	68	73.5	mV
CSP and CSN bias current	I_{CS_BIAS}	$V_{CSP} = V_{CSN} = 0V$		70		μA
IAVGP and IAVGN bias current	I_{AV_BIAS}	$V_{IAVGN} = 5V$, $V_{IAVGN} = 20V$, IAVGP - IAVGN = 40mV		55		μA
Switching Frequency						
Switching frequency	f_{SW}	$FSW = 10$, $V_{OUT} = 5V$	300	400	500	kHz
		$FSW = 00$, $V_{OUT} = 5V$	140	200	260	kHz
Frequency spread spectrum (FSS) span ⁽¹⁰⁾	f_{SS}	DITHER = 1		± 6		% of f_{SW}
FSS modulation frequency ⁽¹⁰⁾	$f_{MODULATION}$	DITHER = 1		2		kHz
Gate Driver						
Gate source current capability ⁽¹⁰⁾	I_{HG_SO}	$V_{CC} = 7.2V$, 4.7nF load		0.7		A
	I_{LG_SO}			0.85		A
Gate sink current capability ⁽¹⁰⁾	I_{HG_SI}	$V_{CC} = 7.2V$, 4.7nF load		1.6		A
	I_{LG_SI}			2		A
Low-side (LS) gate output high voltage	V_{LS_HIGH}		$V_{CC} - 0.05$			V
LS gate output low voltage	V_{LS_LOW}				0.05	V
High-side (HS) gate output high voltage	V_{HS_HIGH}		$V_{BST-SW} - 0.05$			V
HS gate output low voltage	V_{HS_LOW}				0.05	V
Dead time between the HS gate and LS gate ⁽¹⁰⁾	t_{DEAD}			30		ns
Over-Voltage Protection (OVP)						
FB OVP trigger threshold	V_{OVP_RISING}		119	127	135	% of V_{REF}
FB OVP recovery threshold	$V_{OVP_FALLING}$		104	111	118	% of V_{REF}
Thermal Protection						
Thermal shutdown ⁽¹⁰⁾	T_{SD}			150		$^{\circ}C$
Thermal shutdown hysteresis ⁽¹⁰⁾	T_{SD_HYS}			25		$^{\circ}C$

ELECTRICAL CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 12V$, $V_{EN} = 2V$, $T_J = -40^{\circ}C$ to $+125^{\circ}C$ ⁽⁸⁾, typical values are tested at $T_J = 25^{\circ}C$, unless otherwise noted.

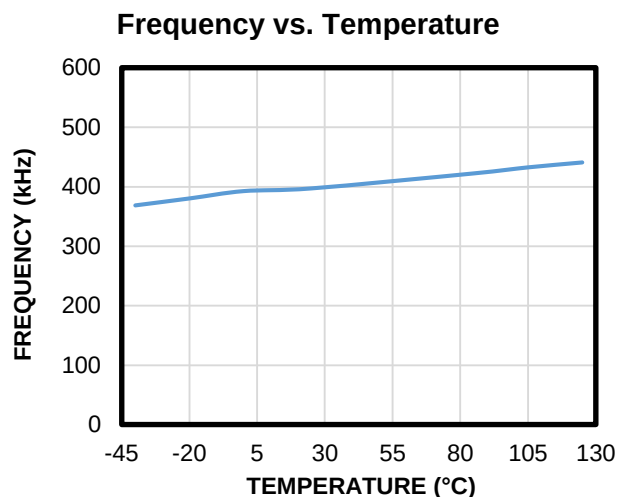
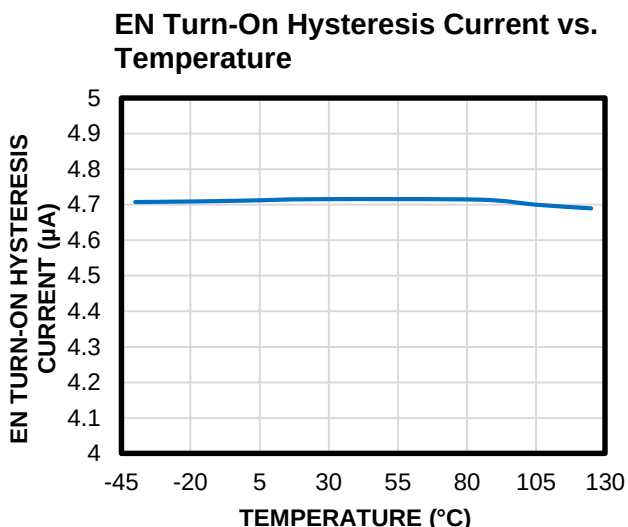
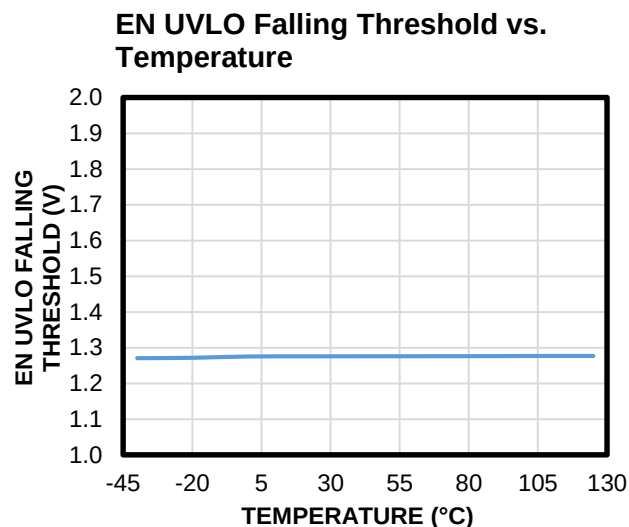
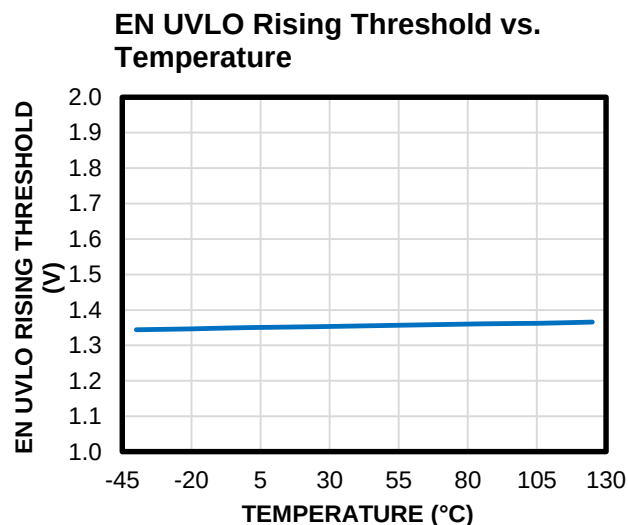
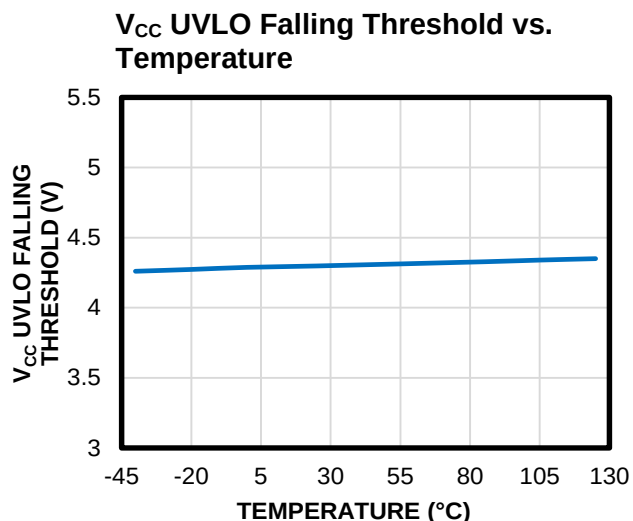
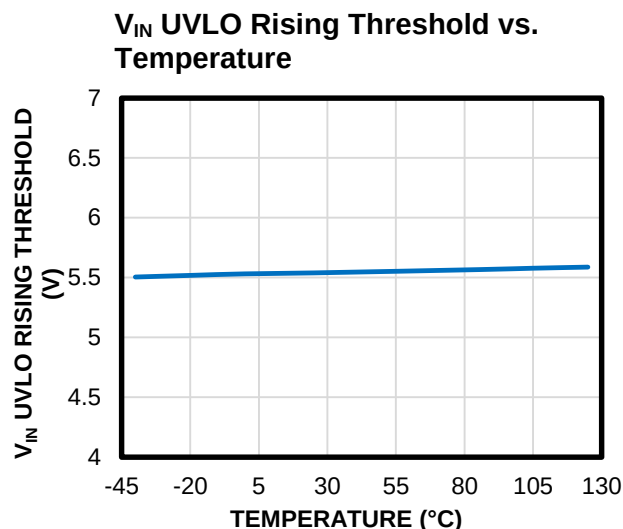
Parameter	Symbol	Condition	Min	Typ	Max	Units
Power Good (PG) (INT Pin)						
PG upper trip threshold	PG _{H_FALLING}	PNG = 1, INT pulls low	110	117	124	% of V _{REF}
	PG _{H_RISING}	PNG = 0, INT pulls high	101	106.5	112	% of V _{REF}
PG lower trip threshold	PG _{L_FALLING}	PNG = 1, INT pulls low	80	85.5	91	% of V _{REF}
	PG _{L_RISING}	PNG = 0, INT pulls high	85	91	97	% of V _{REF}
PG delay (INT response to PNG event)	t _{PG_DELAY}	Low to high		10		μs
		V _{OUT} under-voltage (UV), high to low		2		μs
		V _{OUT} over-voltage (OV), high to low		6.5		μs
INT sink current capability	I _{SINK_INT}	Sink 4mA		0.1	0.4	V
INT leakage current	I _{LKG_INT}	V _{INT} = 5V			1	μA
Digital Interface						
Input logic low voltage	V _{LI}	SCL, SDA			0.8	V
Input logic high voltage	V _{HI}	SCL, SDA	2			V
Logic input current	I _{SCL_SDA_LKG}	SCL/SDA = 5V	-1		+1	μA
Output Logic Low Voltage	V _{LO}	SDA, sink 4mA			0.4	V
ADDR and ILIM Pin Setting Thresholds						
ADDR configuration voltage level 1	V _{ADDR1}	Set digital interface address 60H			0.23	AVDD
ADDR configuration voltage level 2	V _{ADDR2}	Set digital interface address 62H	0.27		0.47	AVDD
ADDR configuration voltage level 3	V _{ADDR3}	Set digital interface address 64H	0.51		0.68	AVDD
ADDR configuration voltage level 4	V _{ADDR4}	Set digital interface address 66H	0.74			AVDD
ADDR/ILIM to ground pull-down resistor				2		MΩ
FS Pin Setting Threshold						
FS configuration voltage level 1	V _{FS1}	FSW = 00	0.51		0.68	AVDD
FS configuration voltage level 2	V _{FS2}	FSW = 10	0.74			AVDD
Current Monitor Function						
IMON output voltage gain	G _{IMON}	5mV I _{AVG} sense voltage		18.8		V/V
		55mV I _{AVG} sense voltage	16.92	18.8	20.68	V/V

Notes:

- 8) Not tested in production. Guaranteed by over-temperature correlation.
- 9) The MP2980 has a 6V minimum start-up voltage, and the V_{IN} UVLO falling threshold is below the V_{CC} UVLO falling threshold.
- 10) Guaranteed by engineer sample characterization.

TYPICAL CHARACTERISTICS

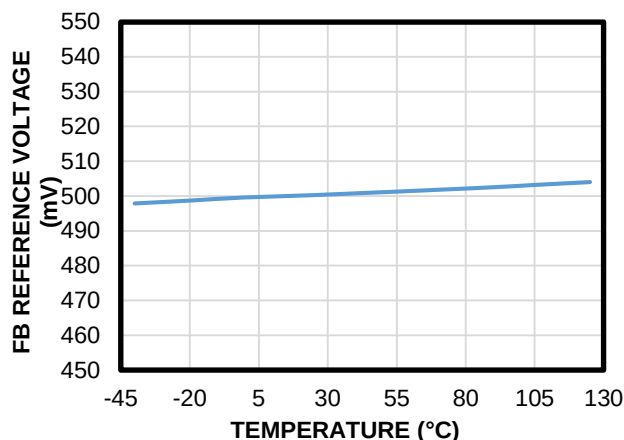
$V_{IN} = 12V$, $V_{OUT} = 5V$, $L = 4.7\mu H$, $T_A = 25^\circ C$, unless otherwise noted.



TYPICAL CHARACTERISTICS (continued)

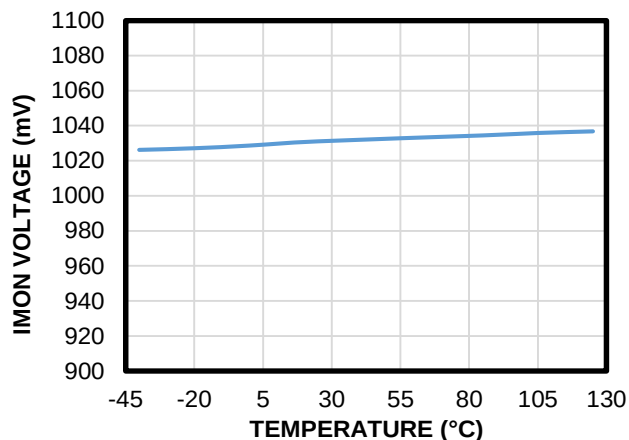
$V_{IN} = 12V$, $V_{OUT} = 5V$, $L = 4.7\mu H$, $T_A = 25^\circ C$, unless otherwise noted.

FB Reference Voltage vs. Temperature

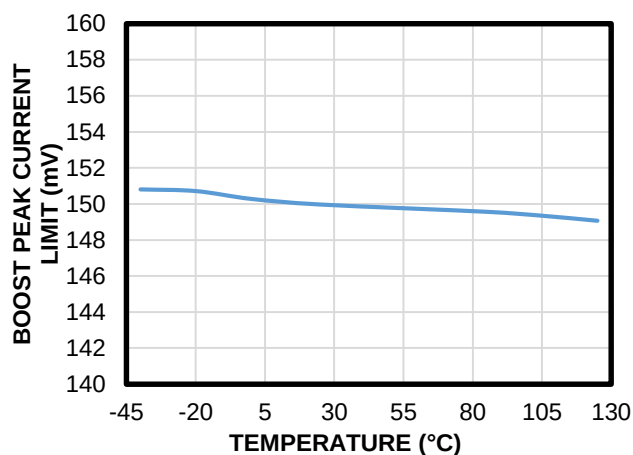


IMON Voltage vs. Temperature

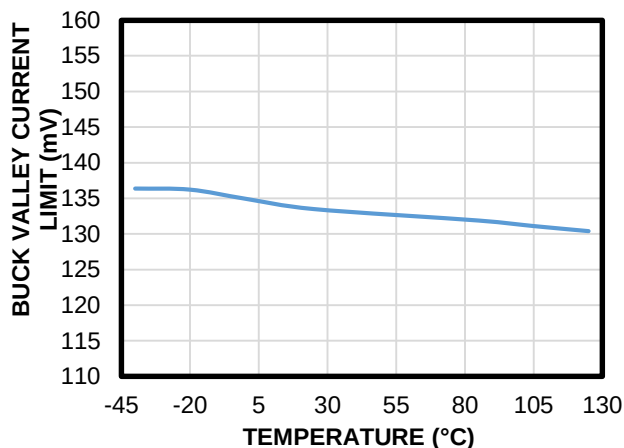
$V_{IAVGP} - V_{IAVGN} = 55mV$



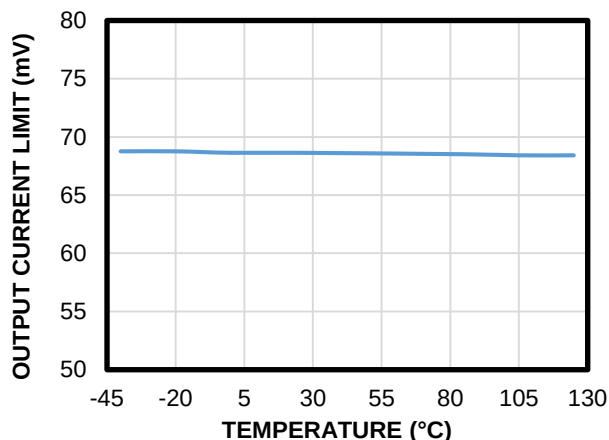
Boost Peak Current Limit vs. Temperature



Buck Valley Current Limit vs. Temperature

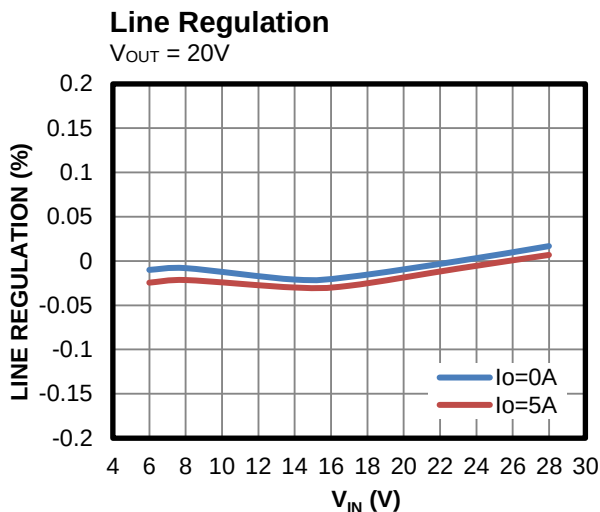
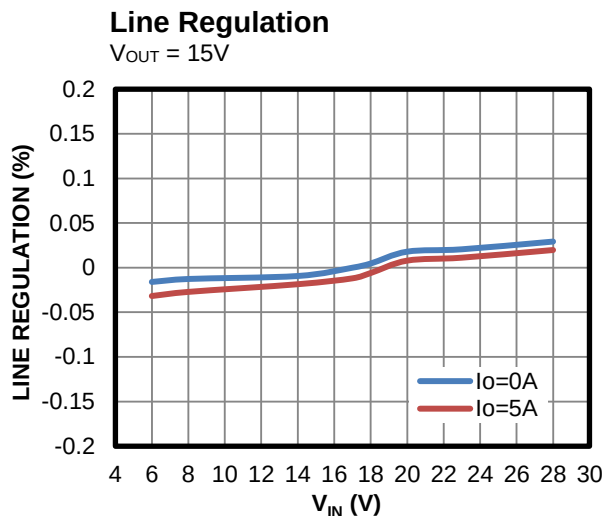
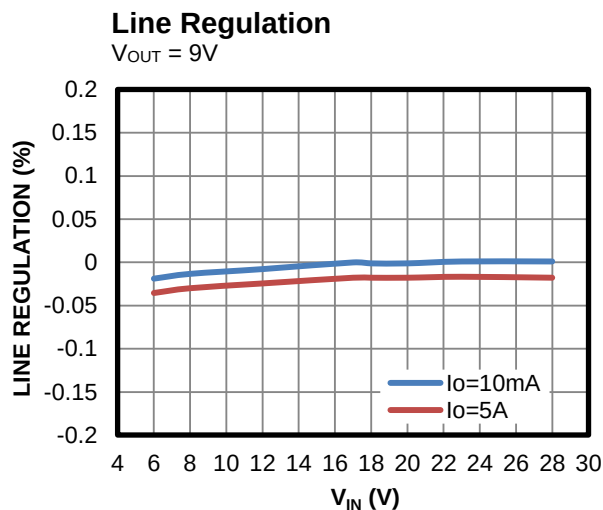
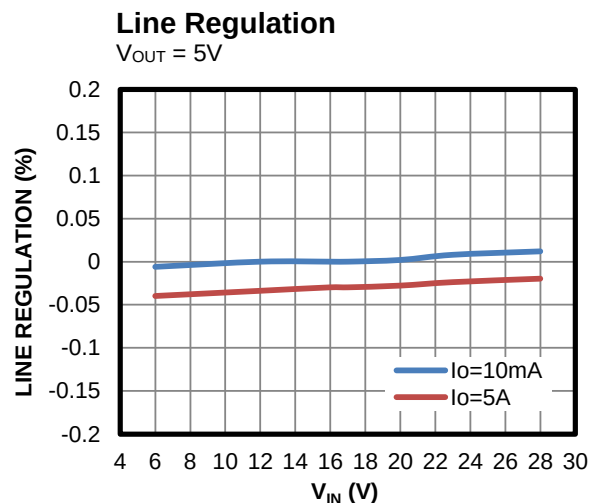
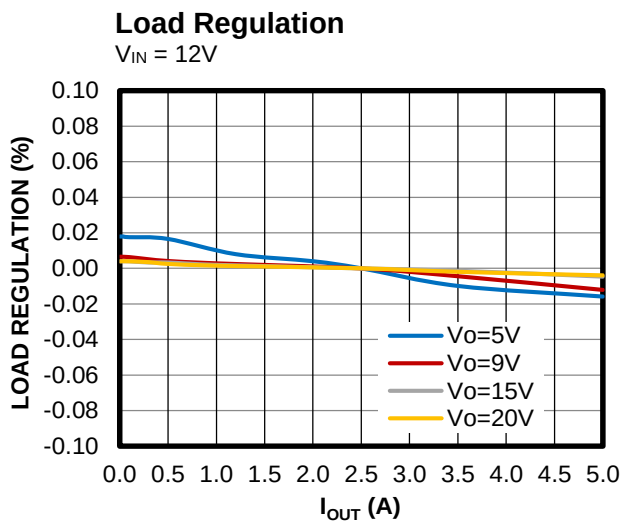
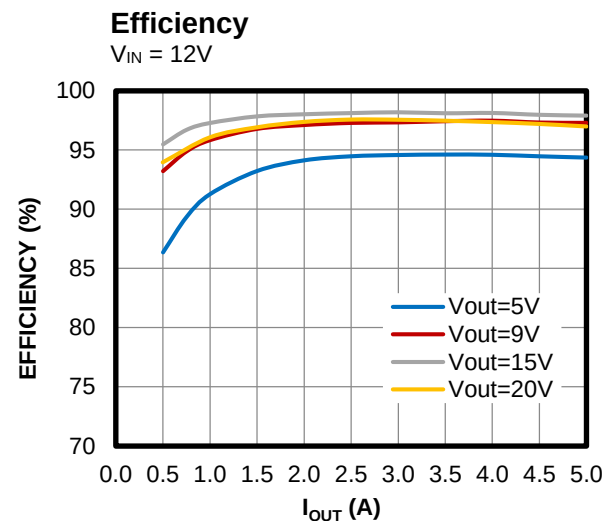


Output Current Limit (ILIM = 111) vs. Temperature



TYPICAL PERFORMANCE CHARACTERISTICS

$V_{IN} = 12V$, $V_{OUT} = 5V$, $L = 4.7\mu H$, $T_A = 25^\circ C$, unless otherwise noted.

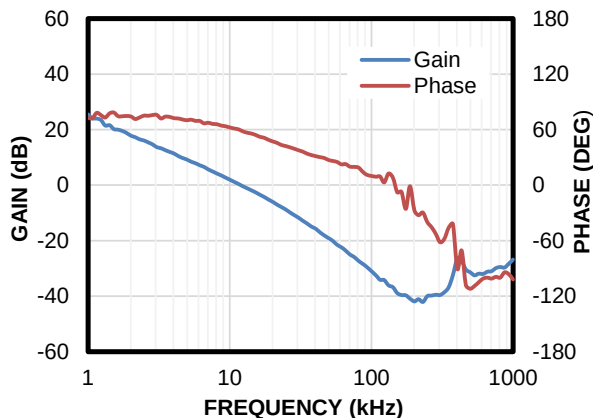


TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $L = 4.7\mu H$, $T_A = 25^\circ C$, unless otherwise noted.

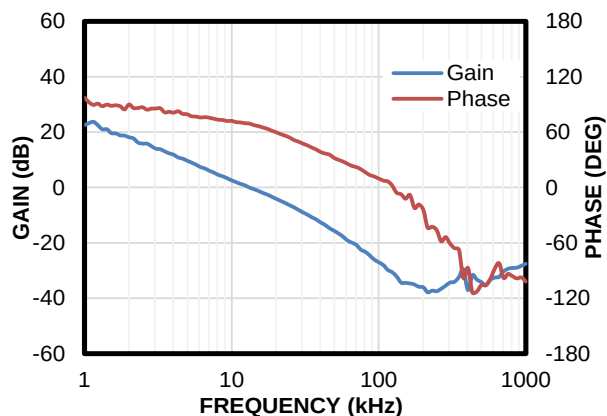
Bode Plot

$V_{OUT} = 5V$, $I_{OUT} = 3A$, $BW = 12.37kHz$,
PM = 58.149 degrees



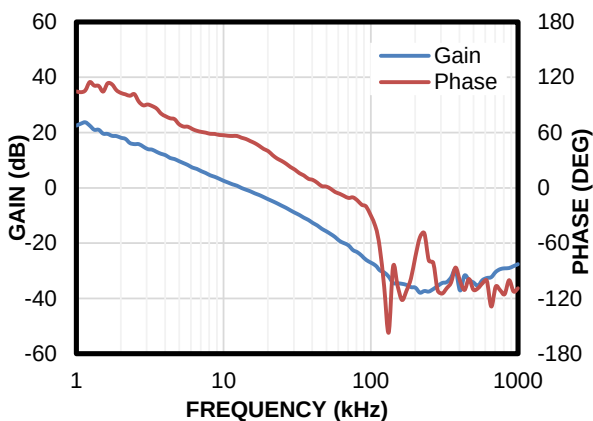
Bode Plot

$V_{OUT} = 9V$, $I_{OUT} = 3A$, $BW = 13.81kHz$,
PM = 68.188 degrees



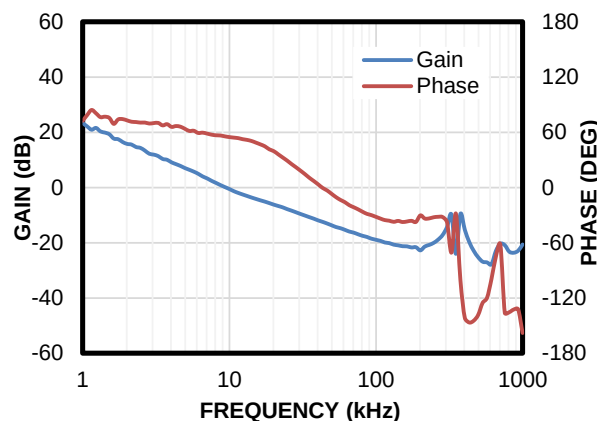
Bode Plot

$V_{OUT} = 15V$, $I_{OUT} = 3A$, $BW = 9.16kHz$,
PM = 57.613 degrees



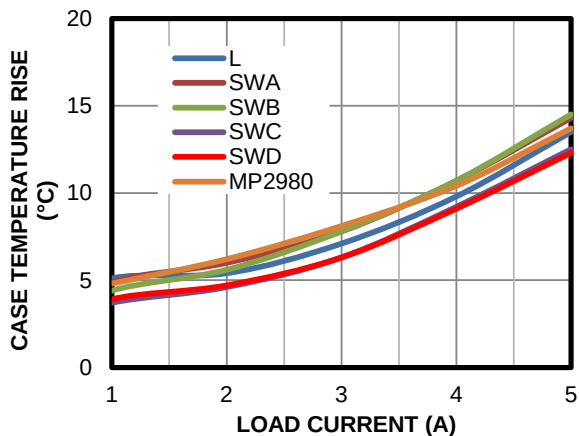
Bode Plot

$V_{OUT} = 20V$, $I_{OUT} = 5A$, $BW = 10kHz$,
PM = 54.907 degrees



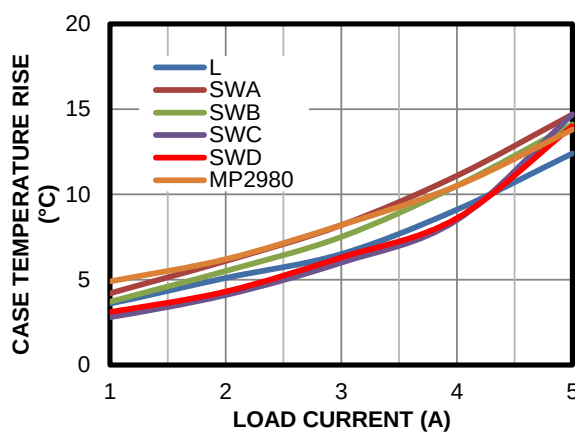
Case Temperature Rise

$V_{IN} = 12V$, $V_{OUT} = 5V$, $FSW = 10$, based on
the EV2980-R-00A



Case Temperature Rise

$V_{IN} = 12V$, $V_{OUT} = 9V$, $FSW = 10$, based on
the EV2980-R-00A

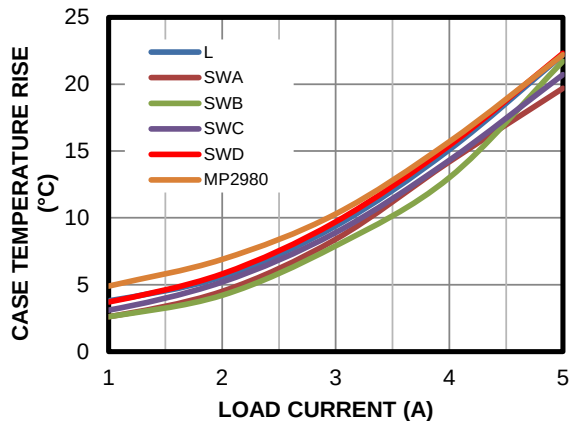


TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

$V_{IN} = 12V$, $V_{OUT} = 5V$, $L = 4.7\mu H$, $T_A = 25^\circ C$, unless otherwise noted.

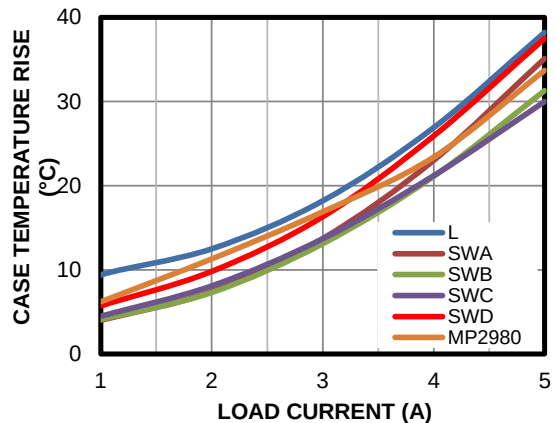
Case Temperature Rise

$V_{IN} = 12V$, $V_{OUT} = 15V$, $FSW = 10$, based on the EV2980-R-00A



Case Temperature Rise

$V_{IN} = 12V$, $V_{OUT} = 20V$, $FSW = 10$, based on the EV2980-R-00A

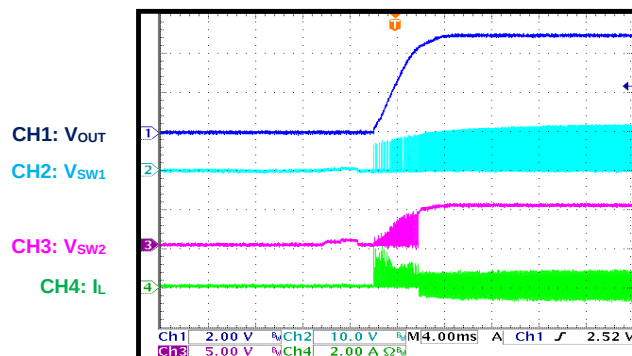


TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $L = 4.7\mu H$, $T_A = 25^\circ C$, unless otherwise noted.

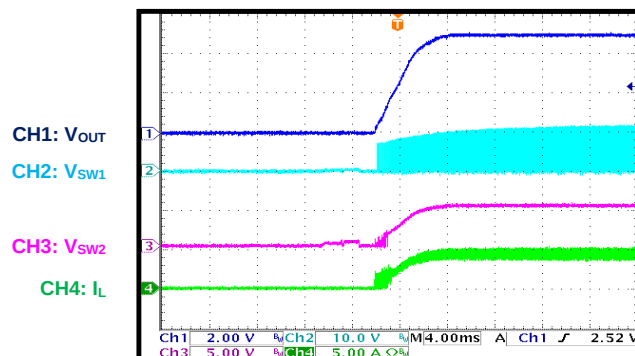
V_{IN} Start-Up

Load = 0A



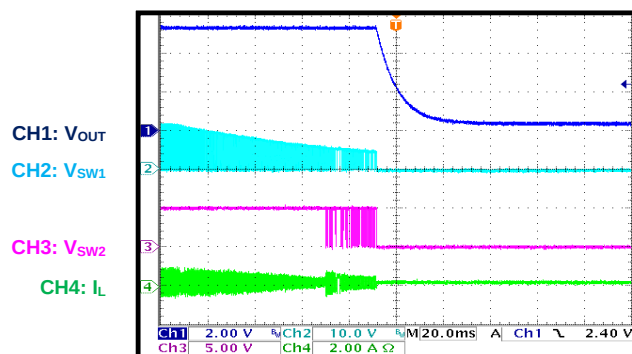
V_{IN} Start-Up

Load = 5A



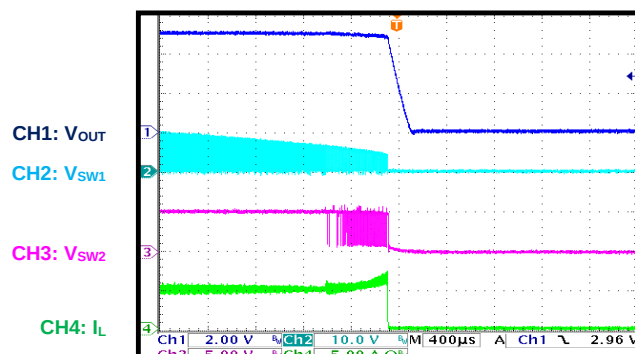
V_{IN} Shutdown

Load = 0A



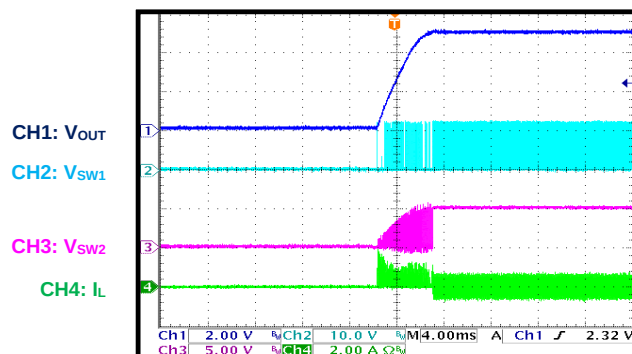
V_{IN} Shutdown

Load = 5A



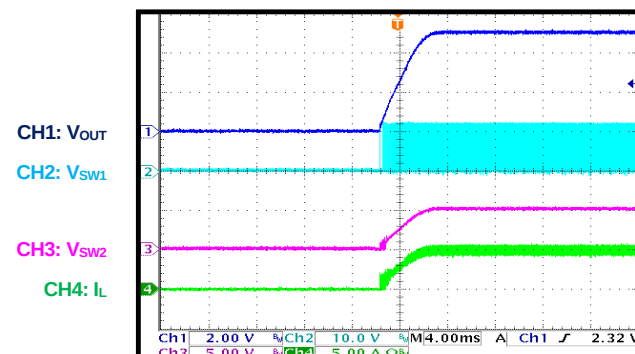
ENPWR Bit Enable via the Digital Interface

Load = 0A



ENPWR Bit Enable via the Digital Interface

Load = 5A

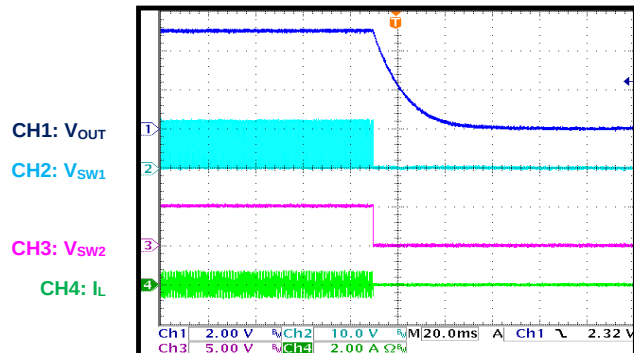


TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

$V_{IN} = 12V$, $V_{OUT} = 5V$, $L = 4.7\mu H$, $T_A = 25^\circ C$, unless otherwise noted.

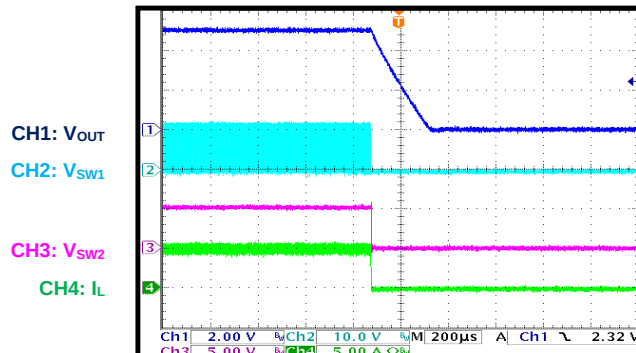
ENPWR Bit Disable via the Digital Interface

Load = 0A



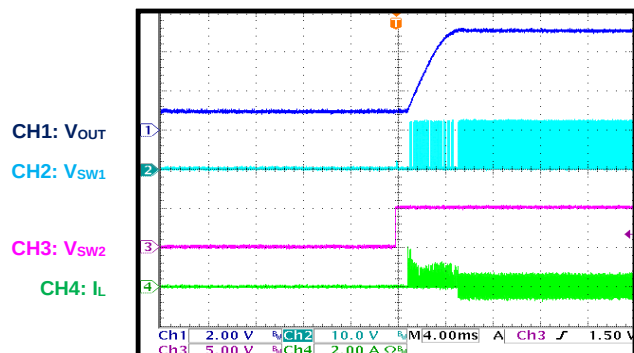
ENPWR Bit Disable via the Digital Interface

Load = 5A



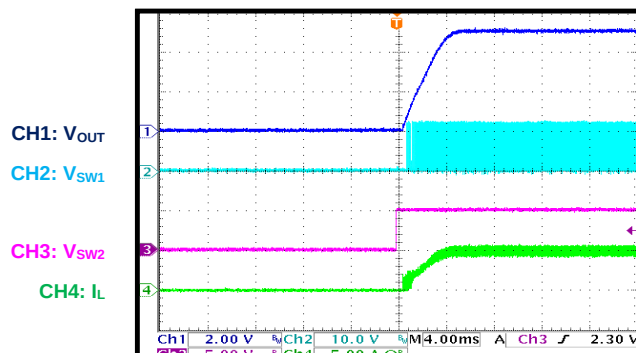
Start-Up through EN

Load = 0A



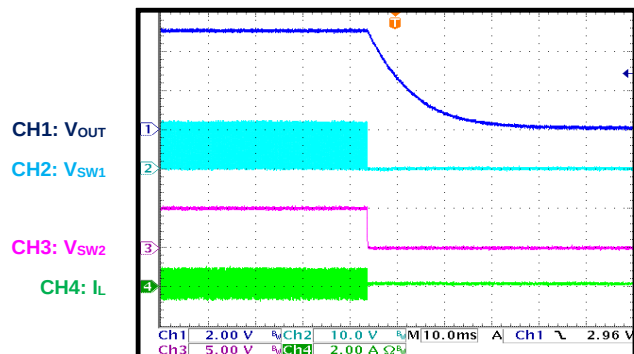
Start-Up through EN

Load = 5A



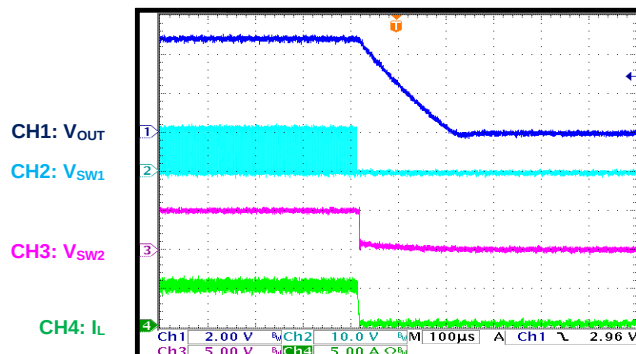
Shutdown through EN

Load = 0A



Shutdown through EN

Load = 5A

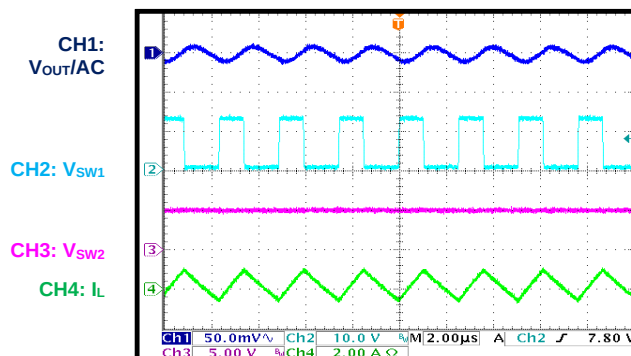


TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $L = 4.7\mu H$, $T_A = 25^\circ C$, unless otherwise noted.

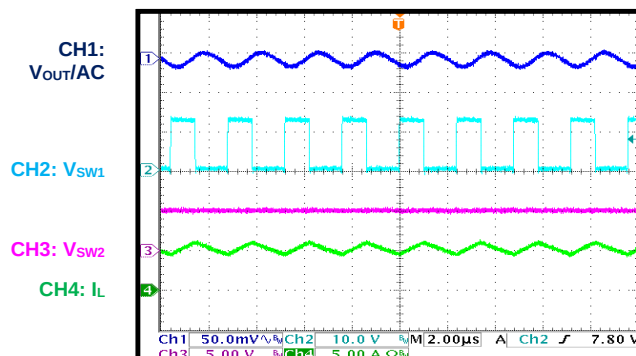
Steady State

$V_{IN} = 12V$, $V_{OUT} = 5V$, $I_{OUT} = 0A$



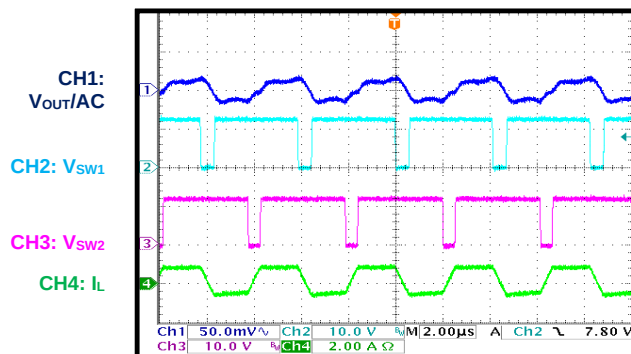
Steady State

$V_{IN} = 12V$, $V_{OUT} = 5V$, $I_{OUT} = 5A$



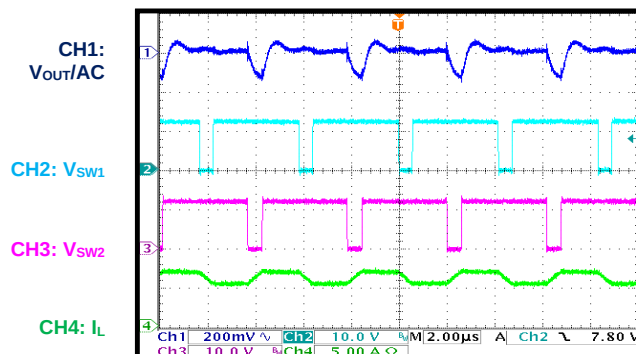
Steady State

$V_{IN} = 12V$, $V_{OUT} = 12V$, $I_{OUT} = 0A$



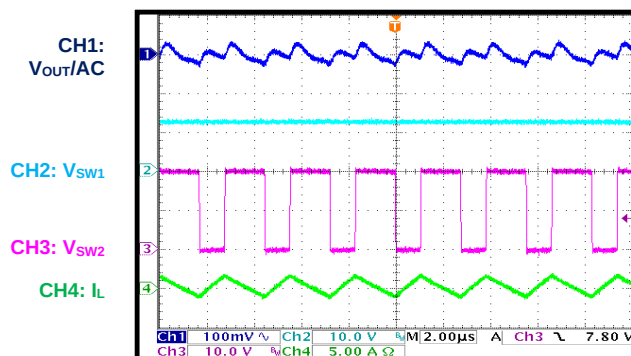
Steady State

$V_{IN} = 12V$, $V_{OUT} = 12V$, $I_{OUT} = 5A$



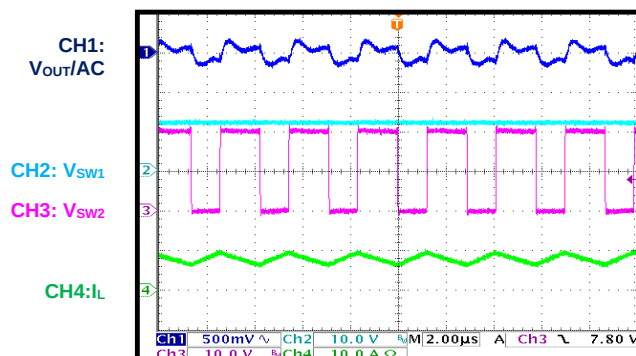
Steady State

$V_{IN} = 12V$, $V_{OUT} = 20V$, $I_{OUT} = 0A$



Steady State

$V_{IN} = 12V$, $V_{OUT} = 20V$, $I_{OUT} = 5A$

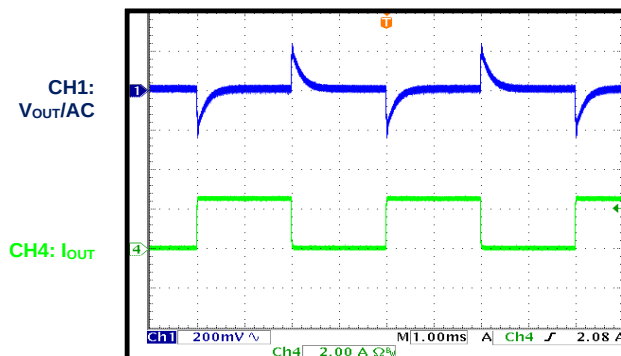


TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

$V_{IN} = 12V$, $V_{OUT} = 5V$, $L = 4.7\mu H$, $T_A = 25^\circ C$, unless otherwise noted.

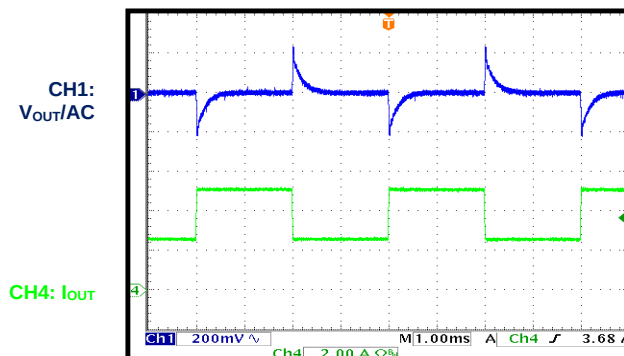
Load Transient

$V_{IN} = 12V$, $V_{OUT} = 5V$, load = 0A to 2.5A,
150mA/ μs



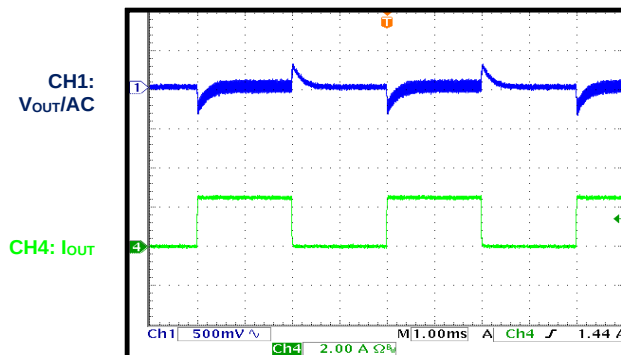
Load Transient

$V_{IN} = 12V$, $V_{OUT} = 5V$, load = 2.5A to 5A,
150mA/ μs



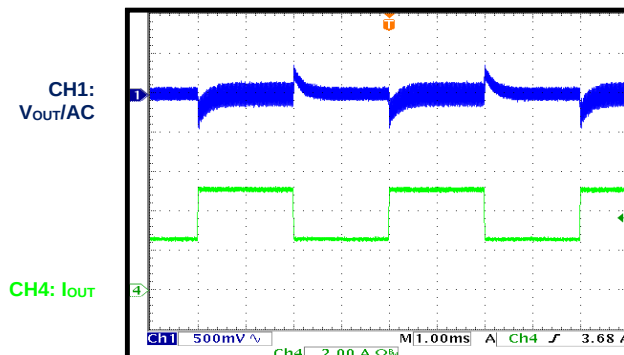
Load Transient

$V_{IN} = 12V$, $V_{OUT} = 20V$, load = 0A to 2.5A,
150mA/ μs



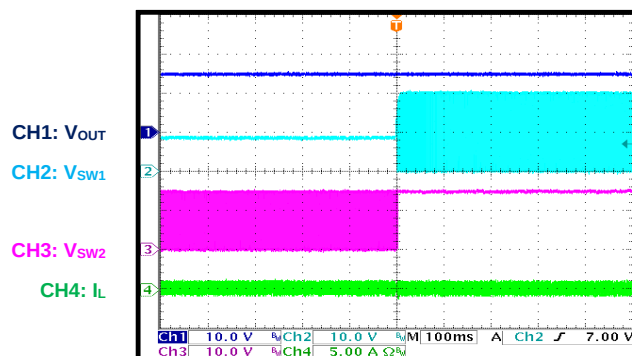
Load Transient

$V_{IN} = 12V$, $V_{OUT} = 20V$, load = 2.5A to 5A,
150mA/ μs



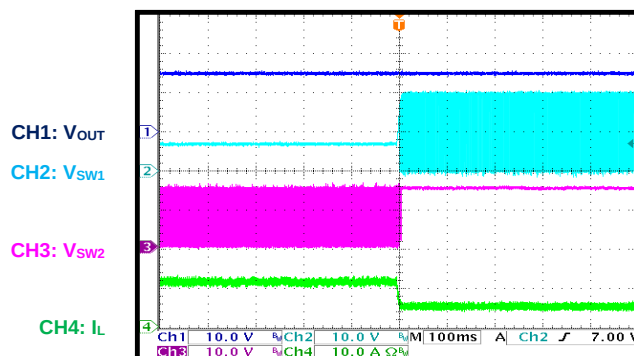
Input Voltage Transient

$V_{IN} = 9V$ to $20V$, $V_{OUT} = 15V$, load = 0A



Input Voltage Transient

$V_{IN} = 9V$ to $20V$, $V_{OUT} = 15V$, load = 5A

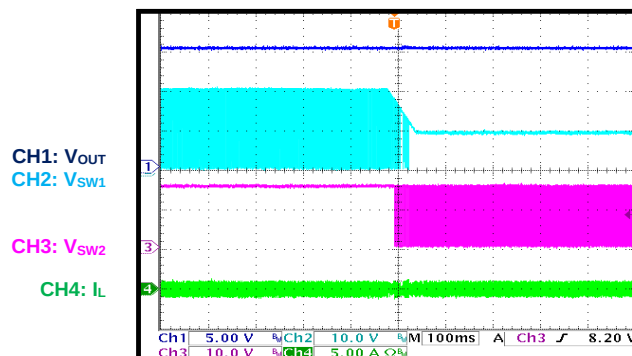


TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $L = 4.7\mu H$, $T_A = 25^\circ C$, unless otherwise noted.

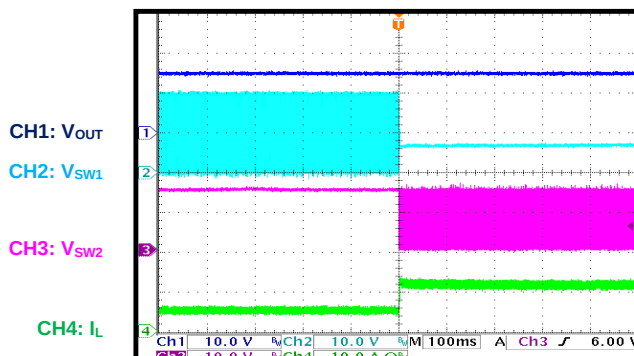
Input Voltage Transient

$V_{IN} = 20V$ to $9V$, $V_{OUT} = 15V$, load = $0A$



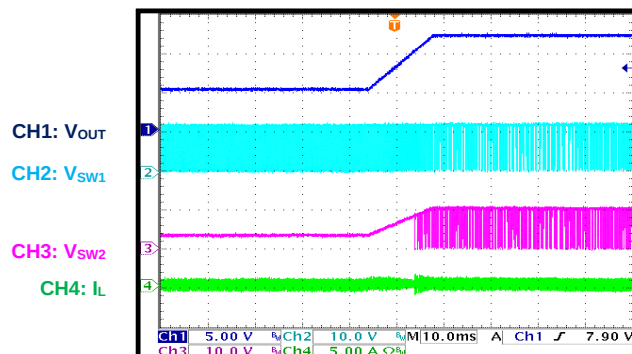
Input Voltage Transient

$V_{IN} = 20V$ to $9V$, $V_{OUT} = 15V$, load = $5A$



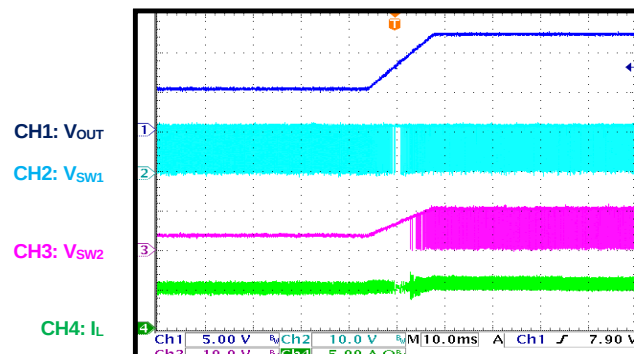
Output Voltage Transient

$V_{OUT} = 5V$ to $12V$, $I_{OUT} = 0A$



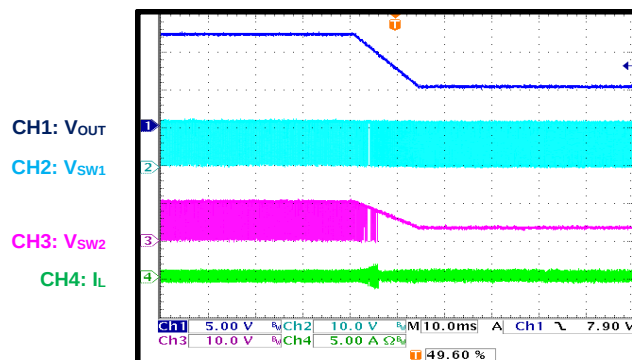
Output Voltage Transient

$V_{OUT} = 5V$ to $12V$, $I_{OUT} = 5A$



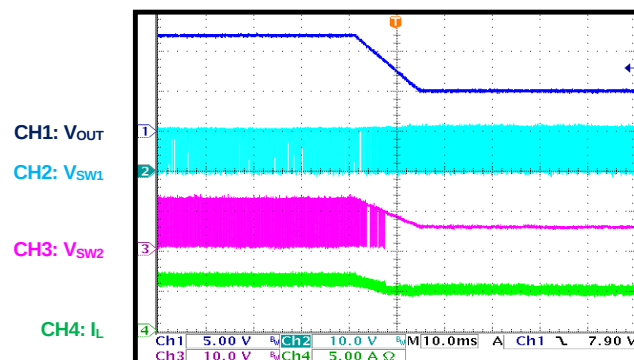
Output Voltage Transient

$V_{OUT} = 12V$ to $5V$, load = $0A$



Output Voltage Transient

$V_{OUT} = 12V$ to $5V$, $I_{OUT} = 5A$

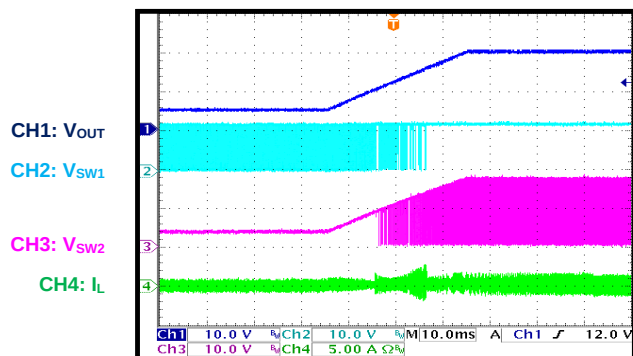


TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

$V_{IN} = 12V$, $V_{OUT} = 5V$, $L = 4.7\mu H$, $T_A = 25^\circ C$, unless otherwise noted.

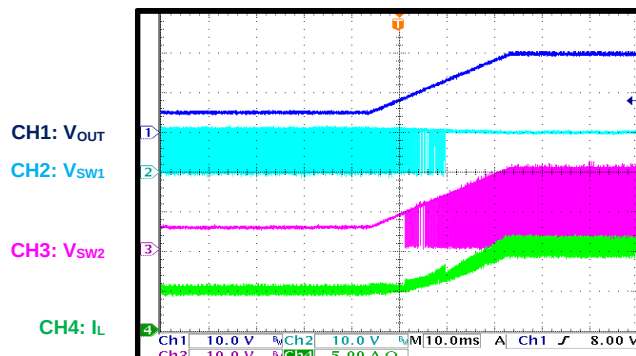
Output Voltage Transient

$V_{OUT} = 5V$ to $20V$, load = $0A$



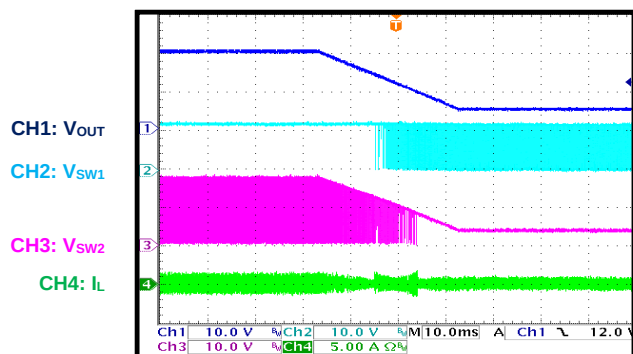
Output Voltage Transient

$V_{OUT} = 5V$ to $20V$, load = $5A$



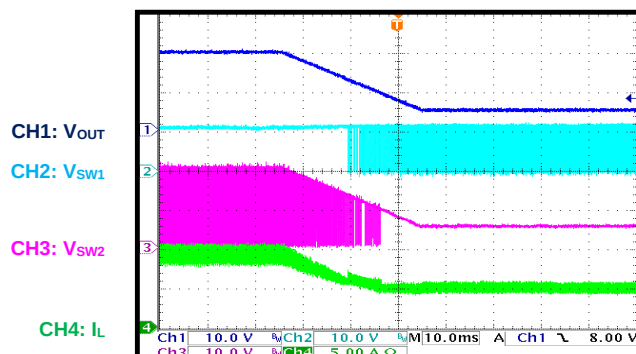
Output Voltage Transient

$V_{OUT} = 20V$ to $5V$, load = $0A$

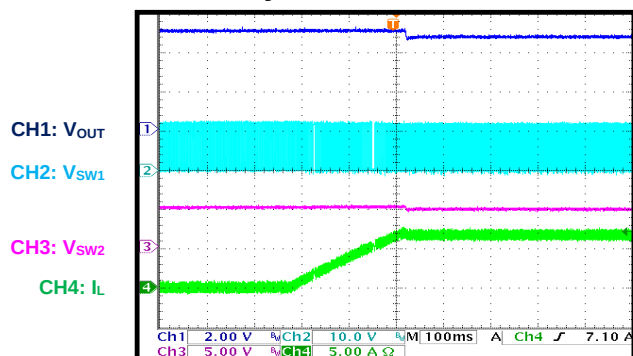


Output Voltage Transient

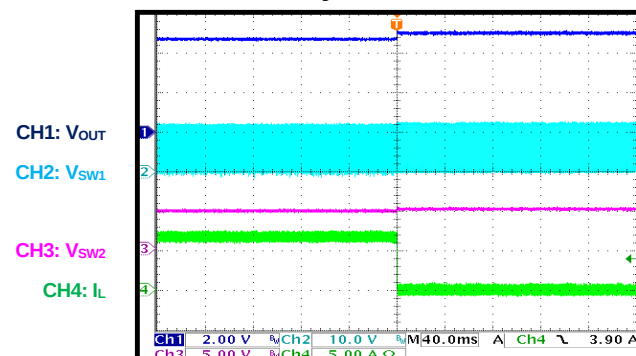
$V_{OUT} = 20V$ to $5V$, load = $5A$



OCP Entry



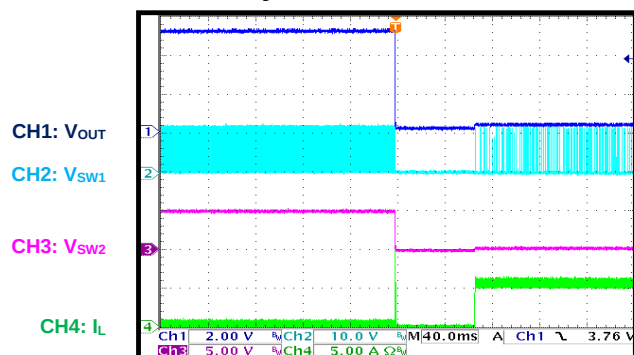
OCP Recovery



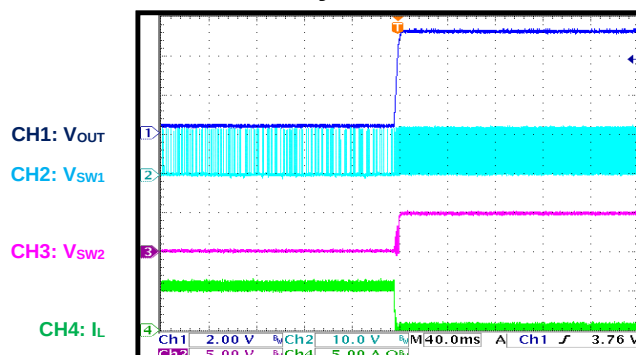
TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

$V_{IN} = 12V$, $V_{OUT} = 5V$, $L = 4.7\mu H$, $T_A = 25^\circ C$, unless otherwise noted.

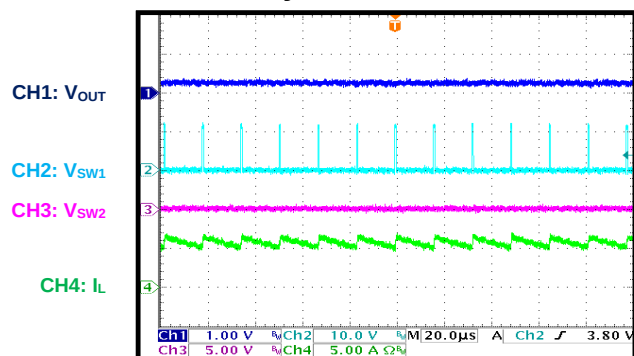
SCP Entry



SCP Recovery



SCP Steady State



FUNCTIONAL BLOCK DIAGRAM

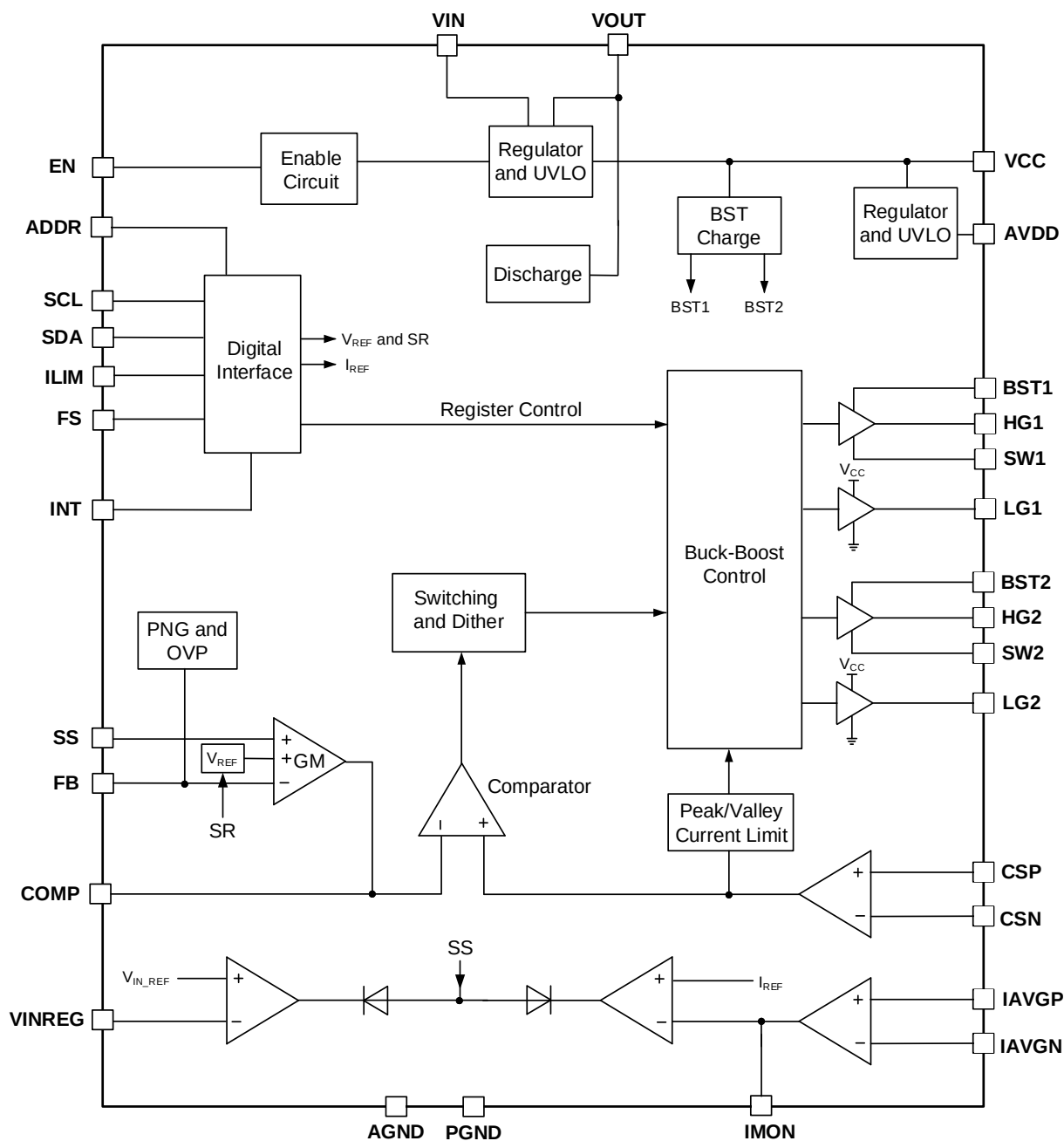


Figure 2: Functional Block Diagram

OPERATION

The MP2980 is a four-switch buck-boost controller. It works with fixed frequency in buck, boost, and buck-boost modes. One special buck-boost control strategy provides high efficiency across the full input voltage (V_{IN}) range and smooth transients between different modes. Figure 2 on page 23 shows the functional block diagram, and the sections below describe the MP2980's functions.

Buck-Boost Operation

The MP2980 can regulate the output voltage (V_{OUT}) above, equal to, or below V_{IN} . Figure 3 shows the single inductor, four-switch power structure using a buck-boost topology.

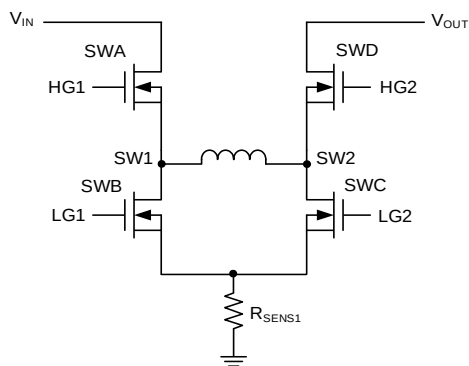


Figure 3: Buck-Boost Topology

Using the buck-boost topology, the MP2980 can operate in buck mode, boost mode, or buck-boost mode with different V_{IN} inputs (see Figure 4).

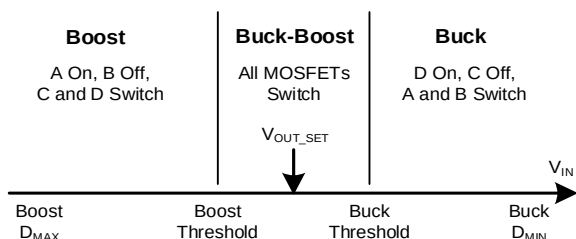


Figure 4: Buck-Boost Operating Range

Buck Mode ($V_{IN} > V_{OUT}$)

If V_{IN} exceeds V_{OUT} significantly, the MP2980 works in buck mode. SWA and SWB switch during buck regulation, SWC is off, and SWD remains on to conduct the inductor current (I_L).

In each cycle of buck mode, SWA turns on when the FB voltage (V_{FB}) drops below the reference

voltage (V_{REF}). After SWA turns off, SWB turns on to conduct I_L until it triggers the COMP control signal. By repeating this operation, the controller regulates V_{OUT} .

Boost Mode ($V_{IN} < V_{OUT}$)

If V_{IN} drops below V_{OUT} significantly, the MP2980 works in boost mode. In this mode, SWC and SWD switch for boost regulation, SWB is off, and SWA remains on to conduct I_L .

In each cycle of boost mode, SWC turns on to conduct I_L . If I_L rises and triggers the control signal on COMP, then SWC turns off and SWD turns on for the freewheeling current. Then SWC turns on and off repeatedly to regulate V_{OUT} in boost mode.

Buck-Boost Mode ($V_{IN} \approx V_{OUT}$)

If V_{IN} is close to V_{OUT} , the controller cannot provide sufficient energy to the load in buck mode due to SWA's minimum off time, or the controller supplies too much power to the load in boost mode due to SWC's minimum on time. Under these conditions, the MP2980 adopts buck-boost control to regulate the output.

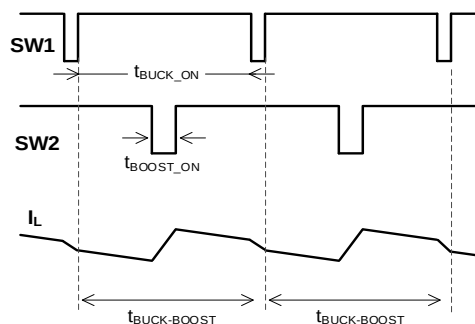


Figure 5: Buck-Boost Waveform

If V_{IN} is close to V_{OUT} , the MP2980 enters buck-boost mode, and a boost switching period is inserted into each buck switching period. The MOSFETs start up in the following sequence:

1. SWA and SWD
2. SWA and SWC
3. SWA and SWD
4. SWB and SWD

Then I_L can meet the required COMP voltage (V_{COMP}) and supply sufficient current to the output.

Power Supply

The MP2980's internal circuit is powered by AVDD at 5.2V, and the gate drivers are powered by VCC at 7.2V. VCC is regulated from V_{IN} and V_{OUT} , while AVDD is powered by V_{CC} .

When V_{IN} is supplied and EN is pulled high, the MP2980 tries to regulate VCC at 7.2V. At the same time, AVDD is regulated at 5.2V. If the AVDD voltage (V_{AVDD}) exceeds the under-voltage lockout (UVLO) threshold and the ENPWR bit is high, the device starts switching and regulates V_{OUT} with soft-start control. If V_{IN} and V_{OUT} both exceed 8.8V, the device powers VCC using the lower voltage source between V_{IN} and V_{OUT} to reduce power loss. Otherwise, the device powers VCC using the higher voltage power source between V_{IN} and V_{OUT} to generate sufficient V_{CC} . VCC and BST have separate UVLO thresholds that keep the gate signal off. Both VCC and BST must have sufficient voltage to enable switching, except for the V_{AVDD} UVLO threshold.

The MP2980 operates between a 6V and 36V V_{IN} range. When VCC is powered from V_{OUT} after start-up, the device can operate until V_{IN} drops below 5V.

When the MP2980 shuts down via V_{AVDD} UVLO or the EN signal, the digital interface cannot respond to the host, and COMP is immediately pulled low. The VCC, AVDD, and BST voltages drop slowly with leakage, but all logic is off.

Start-Up

After start-up, the MP2980 starts switching using soft-start control. The soft-start circuit charges current to the SS pin and ramps up the soft-start voltage (V_{SS}) from 0V. V_{SS} is then fed to the error amplifier (EA) to control V_{OUT} . After the soft-start signal rises to the configured V_{REF} (set via the VREF bits), soft start completes and closed-loop regulation starts. V_{SS} rises and clamps at 0.6V above V_{REF} in steady state, unless a protection is triggered.

The MP2980 typically starts up in buck mode since V_{OUT} is below V_{IN} significantly. If there is some bias voltage on VOUT, the device does not switch until the soft-start signal exceeds V_{FB} , which is proportional to the VOUT bias voltage.

During soft start, the IC works in automatic pulse-frequency modulation (PFM) mode. Neither over-voltage protection (OVP) nor over-current protection (OCP) in hiccup mode work during the soft-start period.

Enable (EN) and Configurable Under-Voltage Lockout (UVLO)

The EN pin enables and disables the MP2980. When applying a voltage exceeding the EN high threshold ($>1.1V$), the device starts up some of the internal circuits in micro-power mode. If the EN voltage (V_{EN}) exceeds the turn-on threshold (1.35V), then the MP2980 enables all functions and starts switching. Switching is disabled once V_{EN} drops below its lower threshold ($<1.28V$).

If V_{EN} is below 0.4V, the MP2980 shuts down completely. After shutdown, the device sinks a small amount of current from the input power (typically $<1\mu A$). EN is compatible with voltages up to 40V. For automatic start-up, connect EN directly to V_{IN} . During EN shutdown, the digital interface resets to its default value after a 200ms discharge time.

The MP2980 features a configurable UVLO hysteresis. During start-up, EN sources a $4.7\mu A$ current out of EN once V_{EN} exceeds 1.35V (see Figure 6).

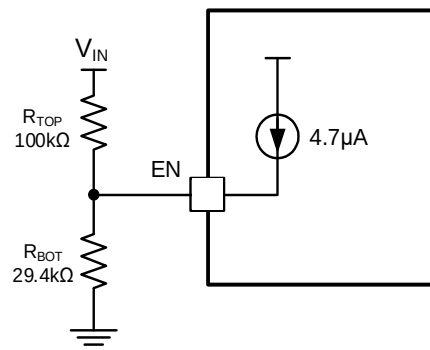


Figure 6: V_{IN} UVLO Configuration

V_{IN} must decrease to exceed the current source and stops switching after the IC starts up. The V_{IN} start switching threshold (V_{IN_ON}) can be calculated with Equation (1):

$$V_{IN_ON} (V) = V_{EN_ON} (V) \times \left(1 + \frac{R_{TOP}}{R_{BOT}}\right) = 5.95V \quad (1)$$

Where V_{EN_ON} is typically about 1.35V.

The V_{IN} stop switching threshold (V_{IN_OFF}) can be calculated with Equation (2):

$$V_{IN_OFF}(V) = V_{EN_OFF}(V) \times \left(1 + \frac{R_{TOP}}{R_{BOT}}\right) - 4.7\mu A \times R_{TOP}(k\Omega) / 1000 = 5.16V \quad (2)$$

Where V_{EN_OFF} is about 1.28V.

Forced Continuous Conduction Mode (FCCM)

The MP2980 works in forced continuous conduction mode (FCCM). The buck on time and boost off time are determined by the internal circuit to obtain a fixed frequency based on the V_{IN} / V_{OUT} ratio. When the load decreases, the average input current drops, and I_L may go negative from V_{OUT} to V_{IN} during the SWD on period. This forces I_L to work in continuous mode with fixed frequency, generating a low V_{OUT} ripple.

Switching Current Limit

The MP2980 senses the low-side MOSFET (LS-FET) current via the CSP and CSN pins. It provides the valley current limit in buck mode and peak current limit in boost mode for each cycle-by-cycle switch. In buck mode, the next period does not start before I_L drops to the valley current limit. As a result, the MP2980 may foldback the frequency when the valley current limit is triggered. The switching current limit can be configured via an external sense resistor. The SWB and SWC current signal is blanked internally for about 180ns to enhance noise rejection.

If the cycle-by-cycle current limit is triggered, then the interrupt OCP bit is set to 1; if the OCP bit is not masked off, then INT is pulled low.

Under an over-current (OC) condition, the MP2980 reaches the cycle-by-cycle current limit. The device may also trigger hiccup protection or latch-off protection, depending on the OCP_MODE bit setting. In hiccup mode, the IC turns off once V_{FB} drops below 60% of V_{REF} . Once the soft-start period finishes, the device reaches the switching current limit. It attempts recovery after a fixed off time that is configured by the SS capacitor (C_{SS}) discharge period. In latch-off mode, the IC turns off if V_{FB} falls below 60% of V_{REF} . Once latch-off protection is triggered, the chip does not recover until a new power cycle is initiated by toggling EN or the ENPWR bit. If the hiccup mode and latch-off

protections are disabled, the IC continues switching with a cycle-by-cycle current limit. The hiccup mode and latch-off protections are masked during the soft-start period.

Based on the cycle-by-cycle switching current limit, the maximum input current (I_{IN_MAX}) in buck mode can be calculated with Equation (3):

$$I_{IN_MAX}(A) = \frac{V_{OUT}}{V_{IN}} \times \eta \times \left(\frac{I_{LIMIT_BUCK}(mV)}{R_{SENSE}(m\Omega)} + \frac{V_{IN} - V_{OUT}}{2 \times L(\mu H) \times f_{SW}(kHz)} \times \frac{V_{OUT}}{V_{IN}} \times 10^3 \right) \quad (3)$$

Where I_{LIMIT_BUCK} is typically 133mV and R_{SENSE} is the cycle-by-cycle switching current limit sense resistor.

I_{IN_MAX} in boost mode can be calculated with Equation (4):

$$I_{IN_MAX}(A) = \frac{I_{LIMIT_BOOST}(mV)}{R_{SENSE}(m\Omega)} - \frac{V_{IN}}{2 \times L(\mu H) \times f_{SW}(kHz)} \times \left(\frac{V_{OUT} - V_{IN}}{V_{OUT}} \times 10^3 \right) \quad (4)$$

Where η is the efficiency, and I_{LIMIT_BOOST} is typically 150mV.

Average Current Limit

The IAVGP and IAVGN pins sense the MP2980's output current (I_{OUT}). A sense resistor can be connected to the VOUT line for average I_{OUT} limit control. Once the sensed signal exceeds the current limit V_{REF} , an internal EA pulls down V_{SS} . Eventually, V_{SS} replaces V_{REF} to control COMP, and I_L is limited by COMP to transfer less energy to the output. Soft start regulates the output low until the average load current drops.

If the switching current is regulated by the average current limit and does not trigger the cycle-by-cycle current limit, the MP2980 does not trigger hiccup mode or latch-off protection, even if the average current limit is reached. This provides constant current charge. If only the average current limit is triggered, the interrupt OCP bit is not set to 1, and INT is not pulled low.

It is recommended to add a 100Ω/220nF current sense filter (see Figure 14 on page 42).

Overload and Short-Circuit Protection (SCP)

If an overload fault occurs, the MP2980 limits I_{OUT} using average current limit loop regulation. If the average current limit loop is disabled, the cycle-by-cycle switching current limit works. Under cycle-by-cycle current limit conditions, if the IC works in boost mode, the SWC peak current is limited. If the IC works in buck mode, SWB remains on until I_L drops to I_{LIMIT_BUCK} , and then the next cycle can begin. Therefore, I_L can be controlled in all work modes.

Output Voltage Regulation

The MP2980 regulates V_{OUT} via the feedback on the FB pin. V_{FB} is compared to the internal reference, which is between 300mV and 2.047V depending on the VREF register bit setting. The EA output on COMP controls I_L to supply V_{OUT} .

Switching Frequency and Frequency Spread Spectrum (FSS)

The MP2980 configures the switching frequency (f_{SW}) via a 2-bit FSW register. f_{SW} is selectable at 200kHz, 300kHz, 400kHz, or 600kHz. A 400kHz f_{SW} is typically recommended.

The MP2980 provides frequency spread spectrum (FSS). If DITHER = 1 (0x02, D[4]), FSS is enabled. If DITHER = 0, FSS is disabled. FSS minimizes peak emissions at certain frequencies (see Figure 7).

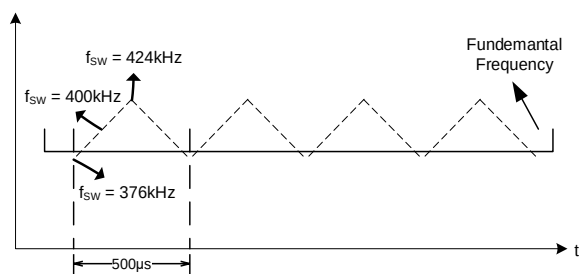


Figure 7: Frequency Spread Spectrum

The MP2980 uses a 2kHz triangle wave to modulate the internal oscillator. The FSS span is $\pm 6\%$.

FSS can be enabled at a f_{SW} of 200kHz, 300kHz, 400kHz, or 600kHz.

Gate Driver and Bootstrap (BST) Power

The MP2980 provides four N-channel MOSFET gate drivers for the H-bridge MOSFETs (see Figure 3 on page 24). Each driver is capable of

sourcing and sinking current. During buck operation, LG1 and HG1 switch while HG2 remains on. During boost operation, LG2 and HG2 switch while HG1 remains on. LG1 and LG2 are powered by the VCC power, and HG1 and HG2 are powered by the BST1 and BST2 power.

Connect capacitors between BST1 and SW1 and between BST2 and SW2 to supply power, which can be provided via an internal diode from VCC or from charging each other.

Over-Voltage Protection (OVP)

The MP2980 monitors the FB pin. If V_{FB} exceeds 127% of V_{REF} and OVP_MODE = 01, then the IC discharges the V_{OUT} capacitor via an internal discharge resistor. It stops discharging when V_{FB} drops to 111% of the regulation voltage. If OVP_MODE = 00, there is no logic to stop switching, even if V_{FB} exceeds the OVP threshold. If OVP_MODE = 10, the IC latches off when V_{OUT} rises to 127% of V_{REF} .

Interrupt (INT Pin)

The INT pin indicates interrupt for the following fault events: OCP (also the switching peak cycle-by-cycle current limit), FB OVP, over-temperature protection (OTP), and V_{OUT} power not good (PNG) reporting.

When any of these faults is triggered, the corresponding register bit is set to 1. At the same time, INT pulls low to indicate an interrupt signal, depending on the related mask register setting.

INT is an open-drain output. When the MP2980 is disabled, INT is an open drain.

Current Monitor Output

The MP2980 senses the average load current via a sense resistor and outputs a voltage signal on the IMON pin. The signal is amplified by the difference between the IAVGP pin voltage (V_{IAVGP}) and IAVGN pin voltage (V_{IAVGN}). It is recommended to connect a small capacitor between IMON and AGND. The IMON output voltage (V_{IMON}) can be calculated with Equation (5):

$$V_{IMON} \text{ (mV)} = \text{GAIN} \times I_{OUT} \text{ (A)} \times R_{SENS} \text{ (m}\Omega\text{)} \quad (5)$$

The IMON gain is typically 18.8V/V. R_{SENS} is the average load current sense resistor.

Configurable Soft-Start Time (SS Pin)

The MP2980 provides a SS pin to configure the soft-start time (t_{SS}). The soft-start charge current (I_{SS}) is typically about 6 μ A. t_{SS} can be estimated with Equation (6):

$$t_{SS}(\text{ms}) = C_{SS}(\text{nF}) \times V_{REF}(\text{V}) / I_{SS}(\mu\text{A}) \quad (6)$$

Where I_{SS} is typically about 6 μ A, C_{SS} is 47nF, and V_{REF} is 0.5V. t_{SS} is about 3.9ms.

Slew-Rate Control and Output Discharge

The MP2980 sets the V_{REF} change slew-rate via the internal SR bits. There are four V_{REF} change (rising and falling) slew rates that can be selected based on the application specifications: 38mV/ms, 50mV/ms, 75mV/ms, or 150mV/ms.

During voltage transients, the discharge function works when GO-BIT = 1. The discharge function is automatically disabled after GO_BIT resets to 0, meaning the V_{REF} change completes. If V_{OUT} has not been discharged to the target voltage when the V_{REF} change completes due to excess output capacitance, the OVP discharge function or the DISCHG bit can be used to continue discharging C_{OUT} .

The output discharge function can be enabled by any of the conditions below:

1. If GO_BIT = 1 and discharge works until a 20ms delay passes after GO_BIT resets to 0.
2. DISCHG = 1.
3. If OVP_MODE = 01 and V_{FB} exceeds 127% of V_{REF} .
4. If the ENPWR bit shuts down and discharge works until a 200ms delay passes.
5. If the EN pin is off and discharge works until a 200ms delay passes.
6. If the V_{IN} UVLO threshold is triggered but AVDD has residual voltage, the MP2980 discharges for 200ms. This discharge function may pause if V_{AVDD} drops.

Current Limit Control (ILIM Pin)

During start-up, the ILIM pin status is latched to the register and sets the default value of the ILIM bits. After start-up, changes in the pin status do not affect the register status unless the pin setting is adjusted and the IC is restarted.

Frequency Control (FS Pin)

During start-up, the FS pin status is latched to the register and sets the default value of the FSW bits. After start-up, changes in the pin status do not affect the register status unless the pin setting is adjusted and the IC is restarted.

VIN Regulation Loop (VINREG Pin)

The VINREG pin sets the minimum operating V_{IN} . If V_{IN} drops to the configured level, the MP2980 pulls down SS and decreases I_{OUT} to maintain V_{IN} . If V_{IN} drops below the VINREG threshold, the MP2980 stops converting power to V_{OUT} .

Thermal Protection

The MP2980 integrates a temperature monitor circuit. If the junction temperature (T_J) exceeds 150°C, the MP2980 shuts down. Once the temperature drops below 125°C, the IC resumes normal operation. If OTP is triggered and INT is not masked, the pin is pulled low.

Digital Interface

The MP2980 integrates a digital interface. The four device addresses are defined as 1100xxx, set via the ADDR resistor divider from AVDD. The R/W bits follow the 7-bit address, where 0 indicates a write command and 1 indicates a read command. The device works as a slave and supports standard mode (100kbps) and fast mode (400kbps) communication. The ADDR pin setting also impacts the default value of the ENPWR bit.

Table 1 shows the configurable device address.

Table 1: Device Address Setting

Device Address	R _{TOP}	R _{BOT}	ENPWR Bit Default Value
60h	NS	0 Ω	1
62h	100k Ω	59k Ω	1
64h	68k Ω	100k Ω	0
66h	0 Ω	NS	0

See the Register Description section on page 30 for more details on the digital interface and register control functions.

Digital Interface Transfer Data

Every byte put on the SDA line must be 8 bits long. Each byte must be followed by an acknowledge (ACK) bit. The acknowledge-related clock pulse is generated by the master. The transmitter releases the SDA line (high) during the acknowledge clock pulse. The receiver must pull down the SDA line during the acknowledge clock pulse to ensure that it remains stable (low) during the clock pulse's high period.

Figure 8 shows the format for data transfers. After the start command (S), a slave address is sent. This address is 7 bits long, followed by an eighth data direction bit (R/W). A 0 indicates a transmission (write), and a 1 indicates a request for data (read). A data transfer is always terminated by a stop command (P), which is generated by the master. If the master wants to communicate on the bus, it can generate a repeated start command (Sr) and address another slave without first generating a stop command.

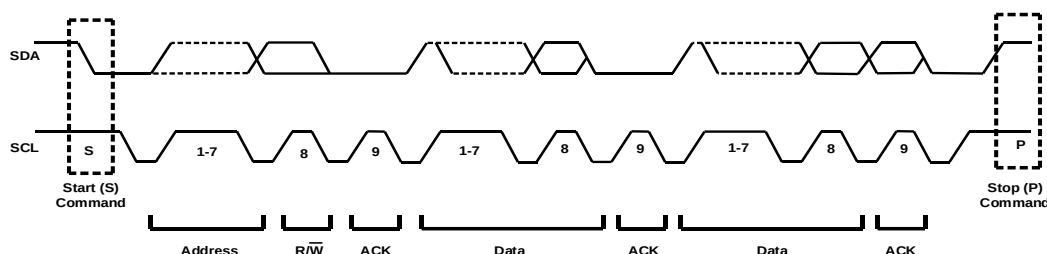
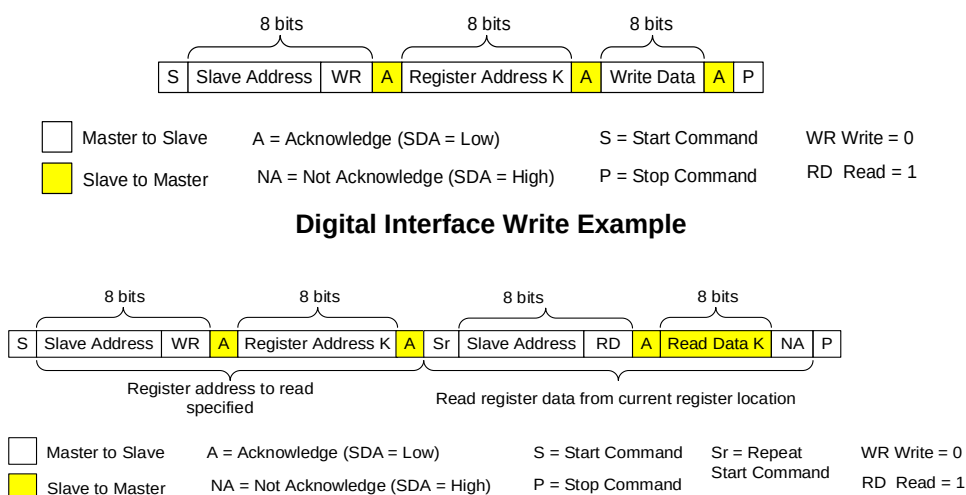


Figure 8: Complete Data Transfer

The MP2980 includes a complete digital interface slave controller. The digital interface slave fully complies with the digital interface specification requirements. It requires a start command, a valid digital interface address, a register address byte, and a data byte for a single data update.

After receiving each byte, the MP2980 acknowledges by pulling the SDA line low during the high period of a single clock pulse. A valid digital interface address selects the MP2980. The MP2980 then performs an update on the falling edge of the LSB byte.

Figure 9 shows an example of the digital interface read and write command.



Digital Interface Read Example
Figure 9: Digital Interface Read and Write

REGISTER DESCRIPTION

Register Map

Addr	Register	Type	D7	D6	D5	D4	D3	D2	D1	D0	Reset State
00h	REF_LSB	R/W	-	-	-	-	-	VREF_L			0000 0100
01h	REF_MSB	R/W	VREF_H								0011 1110
02h	CONTROL1	R/W	SR		DISCHG	DITHER	PNG_LATCH	RESERVED ⁽¹¹⁾	GO_BIT	ENPWR	0100 010x ⁽¹²⁾
03h	CONTROL2	R/W	FSW		-	BB_FSW	OCP_MODE		OVP_MODE		xx00 0101 ⁽¹²⁾
04h	ILIM	R/W	-	-	-	-	-	ILIM			0000 1xxx ⁽¹²⁾
05h	INTERRUPT_STATUS	R/W	-	-	-	OTP	-	OVP	OCP	PNG	0000 0000
06h	INTERRUPT_MASK	R/W	-	-	-	M_OTP	-	M_OVP	M_OCP	M_PNG	0000 0001

Notes:

11) Reserved bit. Do not write values to this bit in application.

12) "x" means that it is determined based on the external pin setting during start-up. See the register function descriptions on page 31 for more details.

REF_LSB (00h)
Format: Direct

The REF_LSB command sets the feedback reference voltage (V_{REF}) low for 3 bits.

Bits	Access	Bit Name	Default	Description
2:0	R/W	VREF_L	3'b 100	Sets the feedback V_{REF} low for 3 bits. LSB = 1mV.

REF_MSB (01h)
Format: Direct

The REF_LSB command sets the feedback V_{REF} high for 8 bits. The FB reference data format requires a total of 11 bits to set V_{REF} . If V_{REF} is an 11-bit, unsigned binary integer of VREF[10:0], then V_{FB} (V) = $V_{REF} / 1000$.

Name	VREF															
Format	Direct, unsigned binary integer															
Register Name	N/A					VREF_H[7:0]								VREF_L[2:0]		
Bit	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0
Access	N/A					R/W	R/W	R/W	R/W	R/W	R/W	R/W	R/W	R/W	R/W	R/W
Function	N/A					Data bit high								Data bit low		
Default Value (0.5V)	N/A					500 integer										

Bits	Access	Bit Name	Default	Description
7:0	R/W	VREF_H	8'b 001111 10	Feedback V_{REF} high 8 bits. LSB = 8mV.

CONTROL1 (02h)
Format: Unsigned binary

The CONTROL1 command sets the V_{REF} changing slew rate, output-to-ground discharge, frequency spread spectrum (FSS), PNG_LATCH, and the V_{REF} change function enable bit.

Bits	Access	Bit Name	Default	Description
7:6	R/W	SR	2'b 01	Configures the V_{REF} changing slew rate. 2'b 00: 38mV/ms 2'b 01: 50mV/ms 2'b 10: 75mV/ms 2'b 11: 150mV/ms This SR control only works after soft start finishes. During the soft-start period, the V_{OUT} slew rate is controlled by soft start. V_{OUT} slew rate = V_{REF} slew rate x feedback ratio Where feedback ratio = $(R1 + R2) / R2$.
5	R/W	DISCHG	1'b 0	Sets the on/off control of the output-to-ground discharge path. 1'b 0: Turn off the discharge path, where the DISCHG bit function works even when the ENPWR bit is low 1'b 1: The MP2980 discharges V_{OUT} via an internal resistor This bit does not affect the output discharge behavior in the following cases: 1. V_{OUT} changed via the digital interface 2. ENPWR bit shutdown 3. EN pin shutdown 4. Output over-voltage protection (OVP) when OVP_MODE enables discharge 5. Trigger V_{IN} UVLO threshold If GO_BIT = 1, the V_{OUT} discharge path automatically turns on. After GO_BIT resets to 0 with a 20ms extra delay, the V_{OUT} discharge path turns off. It is typically recommended to set the slew rate low to allow V_{OUT} to follow the V_{REF} change using this internal discharge current. If V_{OUT} cannot follow the V_{REF} change even with the discharge due to a large output capacitor (C_{OUT}), then there is an additional 20ms of discharge.
4	R/W	DITHER	1'b 0	Enables FSS. 1'b 0: Disable dither 1'b 1: Enable dither
3	R/W	PNG_LATCH	1'b 0	Sets the power not good (PNG) status reset and control. See the PNG bit description on page 35. 1'b 0: The PNG bit status recovers to 0 once V_{OUT} returns to its normal voltage range 1'b 1: The PNG bit status latches to 1 once V_{OUT} exceeds the power good voltage range
2	R/W	RESERVED	1'b 1	Reserved.

1	R/W	GO_BIT	1'b 0	Enables the V_{REF} change function. If GO_BIT = 1, enable the output change based on the VREF register. When the command completes (internal V_{REF} steps to the target V_{REF}), GO_BIT automatically resets to 0. This prevents false operation of V_{OUT} scaling. Write the VREF registers (00h and 01h registers) first, then write GO_BIT = 1. V_{REF} and V_{OUT} change based on the new VREF. GO_BIT resets to 0 when V_{REF} reaches a new level. The host reads GO_BIT to determine whether the V_{REF} scaling is finished. The V_{OUT} discharge path is enabled when GO_BIT = 1, regardless of the DISCHG bit setting. This helps pull V_{OUT} from high to low under light-load conditions. After GO_BIT resets to 0, the discharge continues and turn off after a 20ms delay. 1'b 0: V_{OUT} cannot be changed 1'b 1: V_{OUT} changes based on the VREF registers. After V_{REF} reaches the new level set via the VREF bits, GO_BIT resets to 0 automatically
0	R/W	ENPWR	1'b x	Enables power switching. 1'b 0: Enable power switching 1'b 0: Disable power switching but other internal control circuits work The default value is determined via the ADDR pin setting. See Table 1 on page 28 for more details. If ENPWR resets from 1 to 0, the MP2980 resets the VREF bits to 0.5V (0011 1110 100). The MP2980 resets VREF one-time only to ensure that VREF can be changed to the required value via the digital interface after ENPWR = 0. The host must re-write VREF again if the system requires the previous V_{OUT} value after ENPWR = 0. After ENPWR is set to 0, the discharge function works for 200ms.

CONTROL2 (03h)
Format: Unsigned binary

The CONTROL2 command sets the switching frequency (f_{SW}), buck-boost f_{SW} , over-current protection (OCP), and over-voltage protection (OVP).

Bits	Access	Bit Name	Default	Description
7:6	R/W	FSW	2'b x0	Sets f_{SW}. The default value is determined via the FS pin setting during start-up. See the Electrical Characteristics section on page 8 for the FS pin setting levels. Writable during both ENPWR = 0 and ENPWR = 1 conditions. f_{SW} changes smoothly after the digital interface writes these bits. 2'b 00: 200kHz 2'b 01: 300kHz 2'b 10: 400kHz 2'b 11: 600kHz
4	R/W	BB_FSW	1'b 0	Sets the buck-boost f_{SW}. 1'b 0: Set the buck-boost f_{SW} equal to 40% of the base f_{SW} 1'b 1: Set the buck-boost f_{SW} equal to 80% of the base f_{SW}
3:2	R/W	OCP_MODE	2'b 01	Sets OCP after triggering the cycle-by-cycle switching current limit (valley current limit in buck mode, or peak current limit in boost mode). 2'b 00: No hiccup mode or latch-off protection. I_L is limited by the cycle-by-cycle current limit 2'b 01: Hiccup protection after triggering the switching current limit and FB < 60% of V_{REF}. The off period is controlled by the SS discharge 2'b 10: Latch-off protection. The IC must start up again 2'b 11: Reserved
1:0	R/W	OVP_MODE	2'b 01	Sets OVP protection mode after triggering the threshold at 127% of V_{REF}. 2'b 00: No protection after OVP, where V_{OUT} is regulated by COMP. No discharge after OVP 2'b 01: Discharge V_{OUT} via an internal resistor and stop switching once V_{FB} exceeds 127% of V_{REF}. Recover once V_{FB} drops to 111% of V_{REF} 2'b 10: Latch-off protection. No discharge after OVP 2'b 11: Reserved

ILIM (04h)

Format: Unsigned binary

The ILIM command sets the average current limit.

Bits	Access	Bit Name	Default	Description
2:0	R/W	ILIM	3'b xxx	Sets the average current limit. Can be used to configure the output current (I_{OUT}) limit. The default value is determined via the ILIM pin setting during start-up. Float the ILIM pin to set the ILIM bits = 001. See the Electrical Characteristics section on page 8 for the ILIM pin setting levels. 3'b 000: 27.9mV current limit threshold 3'b 001: 33.3mV current limit threshold 3'b 010: 39.3mV current limit threshold 3'b 011: 45.1mV current limit threshold 3'b 100: 51.2mV current limit threshold 3'b 101: 56.8mV current limit threshold 3'b 110: 62.8mV current limit threshold 3'b 111: 68.7mV current limit threshold

INTERRUPT_STATUS (05h)

Format: Unsigned binary

The INTERRUPT_STATUS command shows the over-temperature protection (OTP), OVP, OCP, and power not good (PNG) events.

Bits	Access	Bit Name	Default	Description	Reset Condition
4	R/W	OTP	1'b 0	Enables the OTP indication. 1'b 0: Normal state 1'b 1: Chip enters OTP state	This bit is latched once triggered. Write 0xFF to this register to reset the interrupt status and INT state.
2	R/W	OVP	1'b 0	Enables the V_{OUT} OVP indication. 1'b 0: Normal state 1'b 1: Chip enters OTP state	
1	R/W	OCP	1'b 0	Enables the cycle-by-cycle switching current limit indication. 1'b 0: Normal state 1'b 1: Cycle-by-cycle current limit is triggered, $V_{FB} < 60\%$ of V_{REF}, and soft start completes	
0	R/W	PNG	1'b 0	Enables the V_{OUT} PNG indicator. 1'b 0: Normal state 1'b 1: Output power is not good. This indicates when V_{OUT} is not within its upper and lower thresholds The PNG_LATCH bit controls the PNG reset behavior.	Related to the PNG_LATCH setting: PNG_LATCH = 0: This bit indicates the instantaneous value. INT indicates the instantaneous state PNG_LATCH = 1: This bit is latched once triggered. Write 0xFF to reset the interrupt status and INT state

INTERRUPT_MASK (06h)
Format: Unsigned binary

The INTERRUPT_MASK command sets the M_OTP, M_OVP, M_OCP, and M_PNG masks.

Bits	Access	Bit Name	Default	Description
4	R/W	M_OTP	1'b 0	1'b 0: Does not mask off the OTP alert 1'b 1: Mask off the OTP alert M_OTP = 1 only masks the INT output. This is similar for other mask bits.
2	R/W	M_OVP	1'b 0	1'b 0: Does not mask off the OVP alert 1'b 1: Mask off the OVP alert M_OVP = 1 only masks the INT output.
1	R/W	M_OCP	1'b 0	1'b 0: Does not mask off the OCP alert 1'b 1: Mask off the OCP alert M_OCP = 1 only masks the INT output.
0	R/W	M_PNG	1'b 1	1'b 0: Does not mask off the PNG alert 1'b 1: Mask off the PNG alert M_PNG = 1 only masks the INT output.

APPLICATION INFORMATION

Output Voltage Setting

The default V_{OUT} is set via a resistor divider connected to FB. The default V_{REF} is 0.5V. The bottom resistor in the resistor divider is typically between 1k Ω and 50k Ω .

The top resistor in the feedback resistor divider ($R1$) can be estimated using Equation (7):

$$R1 = \frac{V_{OUT} - V_{REF}}{V_{REF}} \times R2 \quad (7)$$

It is possible to use the digital interface to select the FB V_{REF} and obtain another V_{OUT} .

Selecting the Inductor

The inductor selection is based on the operation mode. The inductance in buck mode (L_{BUCK}) can be calculated with Equation (8):

$$L_{BUCK} = \frac{V_{OUT}}{f_{SW} \times \Delta I_L} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \quad (8)$$

Where ΔI_L is the peak-to-peak inductor ripple current, which is about 30% to 50% of the maximum load current.

In boost mode, the inductor selection is based on limiting ΔI_L to about 30% to 50% of the maximum input current (I_{IN_MAX}). The target inductance for boost mode (L_{BOOST}) can be calculated with Equation (9):

$$L_{BOOST} = \frac{V_{IN} \times (V_{OUT} - V_{IN})}{V_{OUT} \times f_{SW} \times \Delta I_L} \quad (9)$$

I_{IN_MAX} can be calculated with Equation (10):

$$I_{IN_MAX} = \frac{V_{OUT} \times I_{LOAD_MAX}}{V_{IN} \times \eta} \quad (10)$$

Where I_{LOAD_MAX} is the maximum load current, and η is the efficiency.

Choosing a larger inductance reduces the ripple current but also increases the inductor size and reduces the converter's achievable bandwidth by moving the right half-plane zero to lower frequencies. It is recommended to select the appropriate balance based on the application specifications.

Selecting the Input Capacitor

In buck mode, the MP2980 has a discontinuous input current. In boost mode, the MP2980 has a continuous input current. A capacitor is required to supply the AC current during buck mode while maintaining the DC V_{IN} . For the best performance, place ceramic capacitors as close to V_{IN} as possible. Capacitors with X5R or X7R ceramic dielectrics are recommended due to their stable temperature characteristics. The capacitors must also have a ripple current rating exceeding the converter's maximum input ripple current. The input ripple current in buck mode (I_{CIN_RMS}) can be estimated with Equation (11):

$$I_{CIN_RMS} = I_{OUT} \times \sqrt{\frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)} \quad (11)$$

The worst-case condition in buck mode occurs at $V_{IN} = 2 \times V_{OUT}$, which can be calculated with Equation (12):

$$I_{CIN_RMS} = \frac{I_{OUT}}{2} \quad (12)$$

For simplification, choose an input capacitor (C_{IN}) with an RMS current rating greater than half of the maximum load current.

C_{IN} determines the converter's input voltage ripple (ΔV_{IN}). If there is a ΔV_{IN} requirement in the system, choose C_{IN} to meet the specifications.

In buck mode, ΔV_{IN} can be estimated with Equation (13):

$$\Delta V_{IN} = \frac{I_{OUT}}{f_{SW} \times C_{IN}} \times \frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \quad (13)$$

The worst-case condition occurs at $V_{IN} = 2 \times V_{OUT}$, which can be calculated with Equation (14):

$$\Delta V_{IN} = \frac{1}{4} \times \frac{I_{OUT}}{f_{SW} \times C_{IN}} \quad (14)$$

Selecting the Output Capacitor

In boost mode, I_{OUT} is discontinuous and the output capacitor (C_{OUT}) must be capable of reducing the output voltage ripple (ΔV_{OUT}).

A higher capacitance may be required to decrease ΔV_{OUT} and the transient response. Low-ESR capacitors such as X5R or X7R ceramic capacitors are recommended. If using ceramic capacitors, the capacitance dominates the impedance at f_{SW} . This means ΔV_{OUT} is independent of the ESR. ΔV_{OUT} can be estimated with Equation (15):

$$\Delta V_{OUT} = \frac{(1 - \frac{V_{IN}}{V_{OUT}}) \times I_{LOAD}}{C_{OUT} \times f_{SW}} \quad (15)$$

If using hybrid, polymer, or low-ESR electrolytic capacitors, the ESR dominates the impedance at f_{SW} . ΔV_{OUT} can be estimated using Equation (16):

$$\Delta V_{OUT} = \frac{(1 - \frac{V_{IN}}{V_{OUT}}) \times I_{LOAD}}{C_{OUT} \times f_{SW}} + \frac{I_{LOAD} \times R_{ESR} \times V_{OUT}}{V_{IN}} \quad (16)$$

Where R_{ESR} is the equivalent series resistance of C_{OUT} .

For a 100W USB PD application, a 100 μ F polymer capacitor and four 22 μ F ceramic capacitors are recommended.

Choose C_{OUT} to meet the ΔV_{OUT} and load transient requirements of the design. Consider capacitance derating when designing high V_{OUT} applications.

Selecting the External MOSFET

The MP2980 requires four external N-channel power MOSFETs. Figure 10 shows two for the top switches (switches A and D) and two for the bottom switches (switches B and C). In buck mode, SWA and SWB switch while SWD remains on. In boost mode, SWC and SWD switch while SWA remains on.

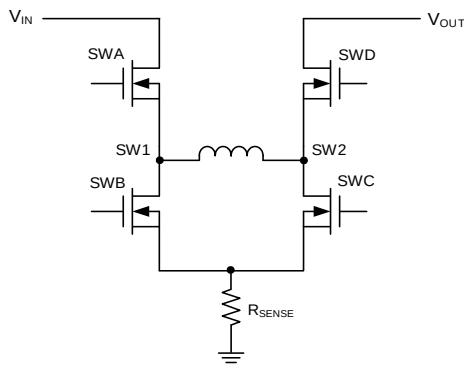


Figure 10: Buck-Boost Topology

There are five critical parameters for selecting a MOSFET, which are described below:

1. Maximum drain-to-source voltage (V_{DS_MAX}): SWA and SWB must withstand the maximum V_{IN} and the transient spikes at SW1 during switching. Therefore, it is recommended to select V_{DS_MAX} for SWA and SWB at $1.5 \times V_{IN}$.
SWC and SWD have V_{OUT} and transient spikes at SW2 during switching. Therefore, it is recommended to select SWC and SWD at $\geq 1.5 \times V_{OUT}$.
2. Maximum continuous drain current (I_{D_MAX}): SWA, SWB, SWC, and SWD must be able to withstand the maximum I_L and peak I_L during switching.
3. MOSFET threshold voltage (V_{TH}): The MP2980's driver voltages are supplied by V_{CC} . The gate plateau voltages of the MOSFETs should be below the converter's minimum V_{CC} , otherwise the MOSFETs may not fully improve during start-up or overload conditions.
4. Total gate charge (Q_G): All switches (Q_G) should be less than 50nC (at a 7.2V gate condition). If there are two MOSFETs in parallel, each MOSFET's Q_G must be smaller than 25nC.
5. Drain-source on resistance ($R_{DS(ON)}$): A lower $R_{DS(ON)}$ is optimal for managing the case temperature rise of the MOSFETs as well as obtaining higher efficiency. See the calculations for the conduction and switching loss for MOSFET SWA, SWB, SWC, and SWD $R_{DS(ON)}$ selection below.

MOSFET SWA

When the MP2980 works in boost mode, SWA remains on. The conduction power loss of SWA ($P_{C_LOSS_SWA}$) can be calculated with Equation (17):

$$P_{C_LOSS_SWA} = (I_{OUT} \times \frac{V_{OUT}}{V_{IN}})^2 \times R_{DS(ON)_SWA} \quad (17)$$

Assume that the MOSFET junction-to-ambient thermal resistance is 50°C/W (determined by the board power dissipation), and that the maximum acceptable temperature rise is 50°C.

The maximum power loss is 1W. $P_{C_LOSS_SWA}$ is estimated relative to the 1W power loss with Equation (18):

$$P_{C_LOSS_SWA} < 1W \quad (18)$$

Based on Equation (18), the MOSFET $R_{DS(ON)}$ can be selected.

When the MP2980 works in buck mode, $P_{C_LOSS_SWA}$ can be calculated with Equation (19):

$$P_{C_LOSS_SWA} = \frac{V_{OUT}}{V_{IN}} \times I_{OUT}^2 \times R_{DS(ON)_SWA} \quad (19)$$

The switching loss of SWA ($P_{SW_LOSS_SWA}$) can be calculated with Equation (20):

$$P_{SW_LOSS_SWA} = \frac{1}{2} \times V_{IN} \times I_{OUT} \times (t_{ON} + t_{OFF}) \times f_{SW} \quad (20)$$

The switch on time (t_{ON}) and the switch off time (t_{OFF}) are based on the MOSFET datasheet information (see Figure 11).

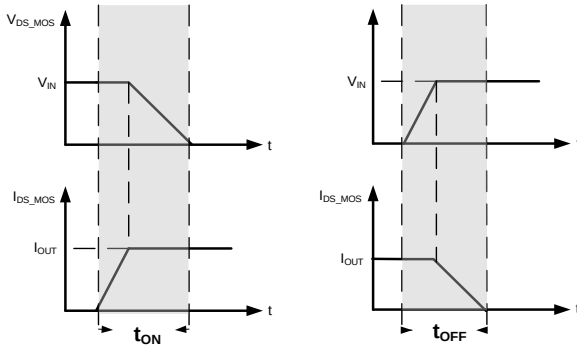


Figure 11: Switch On Time and Switch Off Time

MOSFET SWB

When the MP2980 works in buck mode, its conduction loss ($P_{C_LOSS_SWB}$) can be calculated with Equation (21):

$$P_{C_LOSS_SWB} = (1 - \frac{V_{OUT}}{V_{IN}}) \times I_{OUT}^2 \times R_{DS(ON)_SWB} \quad (21)$$

MOSFET SWC

When the MP2980 works in boost mode, SWB remains off. Its conduction loss in boost mode ($P_{C_LOSS_SWC}$) can be calculated with Equation (22):

$$P_{C_LOSS_SWC} = (1 - \frac{V_{IN}}{V_{OUT}}) \times (I_{OUT} \times \frac{V_{OUT}}{V_{IN}})^2 \times R_{DS(ON)_SWC} \quad (22)$$

When the MP2980 works in boost mode, the SWC switching loss ($P_{SW_LOSS_SWC}$) can be calculated with Equation (23):

$$P_{SW_LOSS_SWC} = \frac{1}{2} \times V_{OUT} \times (I_{OUT} \times \frac{V_{OUT}}{V_{IN}}) \times (t_{ON} + t_{OFF}) \times f_{SW} \quad (23)$$

MOSFET SWD

When the MP2980 works in buck mode, SWD remains on. Its conduction loss ($P_{C_LOSS_SWD}$) can be calculated with Equation (24):

$$P_{C_LOSS_SWD} = I_{OUT}^2 \times R_{DS(ON)_SWD} \quad (24)$$

When the MP2980 works in boost mode, $P_{C_LOSS_SWD}$ can be calculated with Equation (25):

$$P_{C_LOSS_SWD} = (\frac{V_{IN}}{V_{OUT}}) \times (I_{OUT} \times \frac{V_{OUT}}{V_{IN}})^2 \times R_{DS(ON)_SWD} \quad (25)$$

The dead time and the LS-FET switching loss can be ignored.

Compensation Components

The COMP pin controls system stability and transient response. COMP is the output of the internal EA. A series capacitor-resistor combination sets a pole-zero combination to control the control system's characteristics.

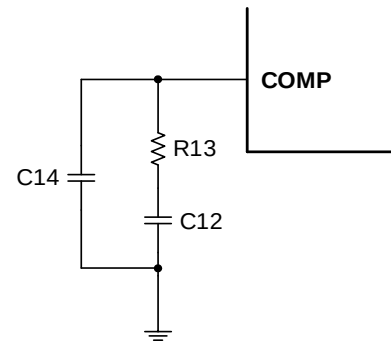


Figure 12: COMP External Compensation

The COMP external compensation sets one pole and one zero (see Figure 12). The pole's frequency (f_{p1}) can be calculated with Equation (26):

$$f_{p1} = \frac{1}{2\pi \times C14 \times R13} \quad (26)$$

The zero's pole (f_{z1}) can be calculated with Equation (27)

$$f_{z1} = \frac{1}{2\pi \times C12 \times R13} \quad (27)$$

When the MP2980 works in buck mode, the DC gain of the voltage feedback loop (A_{VDC}) can be calculated with Equation (28):

$$A_{VDC} = R_{LOAD} \times \frac{G_{CS}}{R_{SENSE}} \times A_{V_EA} \times \frac{V_{FB}}{V_{OUT}} \quad (28)$$

Where A_{V_EA} is the EA voltage gain (300V/V), G_{CS} is the COMP to current-sense gain, R_{SENSE} is the current-sense resistor, and R_{LOAD} is the load resistor.

The system has two important poles. One pole is from the compensation capacitor (C12) and the EA's output resistor. Its frequency (f_{p2}) can be calculated with Equation (29):

$$f_{p2} = \frac{G_{EA}}{2\pi \times C12 \times A_{V_EA}} \quad (29)$$

Where G_{EA} is the EA transconductance (1220 μ A/V).

The second pole is from C_{OUT} and the load resistor. Its frequency (f_{p3}) can be calculated with Equation (30):

$$f_{p3} = \frac{1}{2\pi \times C_{OUT} \times R_{LOAD}} \quad (30)$$

The system may have another significant zero if there is a large output capacitance or high ESR. This zero's frequency (f_{ESR}) can be located with Equation (31):

$$f_{ESR} = \frac{1}{2\pi \times C_{OUT} \times R_{ESR}} \quad (31)$$

When the MP2980 works in boost mode, A_{VDC} can be calculated with Equation (32):

$$A_{VDC} = \frac{V_{IN} \times A_{V_EA} \times R_{LOAD} \times V_{FB} \times G_{CS} \times R13}{2 \times V_{OUT}^2 \times R_{SENSE}} \quad (32)$$

There is also a right-half-plane zero that exists in boost mode. Its frequency (f_{RHPZ}) can be calculated with Equation (33):

$$f_{RHPZ} = \frac{R_{LOAD}}{2 \times \pi \times L} \times \left(\frac{V_{IN}}{V_{OUT}}\right)^2 \quad (33)$$

The right half-plane zero increases the gain and reduces the phase simultaneously, resulting in a smaller phase and gain margin. The worst-case condition occurs when V_{IN} is at its minimum and the output power is at its maximum.

PCB Layout Guidelines

Efficient layout is critical for stable operation. Improper layout may result in reduced performance, EMI issues, resistive loss, and even system instability. For the best results, refer to Figure 13 and follow the steps below:

1. In buck mode, place the input power loop — including the input filter capacitor (C_{IN}), the power MOSFETs (SWA and SWB), and the cycle-by-cycle current sense resistor (R_{SENS1}) — as close as possible.
2. In boost mode, place the output power loop — including the output filter capacitor (C_{OUT}), the power MOSFETs (SWC and SWD), and the cycle-by-cycle current sense resistor (R_{SENS1}) — as close as possible.
3. Use wide copper traces and power loop vias to improve thermal dissipation.
4. Connect the exposed pad to ground.
5. Place vias on the exposed pad for thermal dissipation on the IC.
6. Place small decoupling capacitors close to VIN, VOUT, and AGND.
7. Lay out the gate drive traces and return paths as directly as possible.
8. Lay out the forward and return traces close together to minimize the inductance of the gate drive path. They can either run side by side, or on top of each other on adjacent layers.
9. Use Kelvin connections to R_{SENS2} for the average current sense and R_{SENS1} for the cycle-by-cycle current.
10. Route lines in parallel from the R_{SENS1} and R_{SENSE2} terminals to the IC pins.
11. Avoid crossing noisy areas, such as SW1 and SW2, or gate drive traces.
12. Place the filter capacitor for the current-sense signal as close to the IC pins as possible.
13. Place the VCC and AVDD capacitors as close to the VCC and AVDD pins as possible.
14. Place the BST1 bootstrap capacitor close to the IC, and connect it directly to the BST1 and SW1 pins.

15. Place the BST2 bootstrap capacitor close to the IC, and connect it directly to the BST2 and SW2 pins.
16. To ensure the feedback loop is far from any noise source, place the FB dividers (R1 and R2) as close to the FB and AGND pins as possible.
17. Separate the power and signal paths to ensure that no power or switching current flows through the AGND connections.
18. Connect the PGND and AGND traces near the PGND pin, near the VCC capacitor PGND connection, or near the PGND connection of the cycle-by-cycle current-sense resistor (R_{SENS1}).

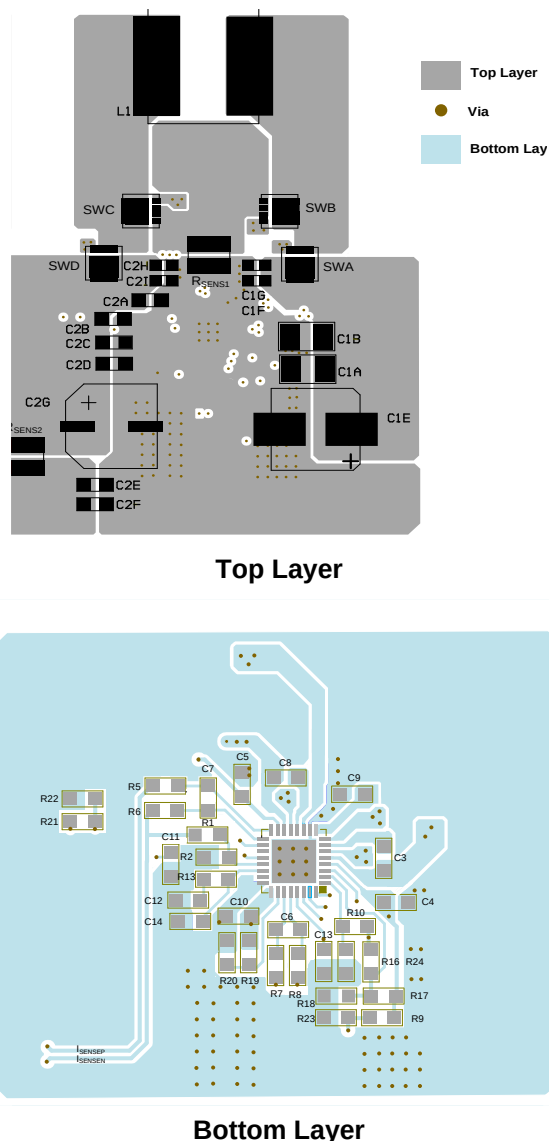


Figure 13: Recommended PCB Layout

TYPICAL APPLICATION CIRCUIT

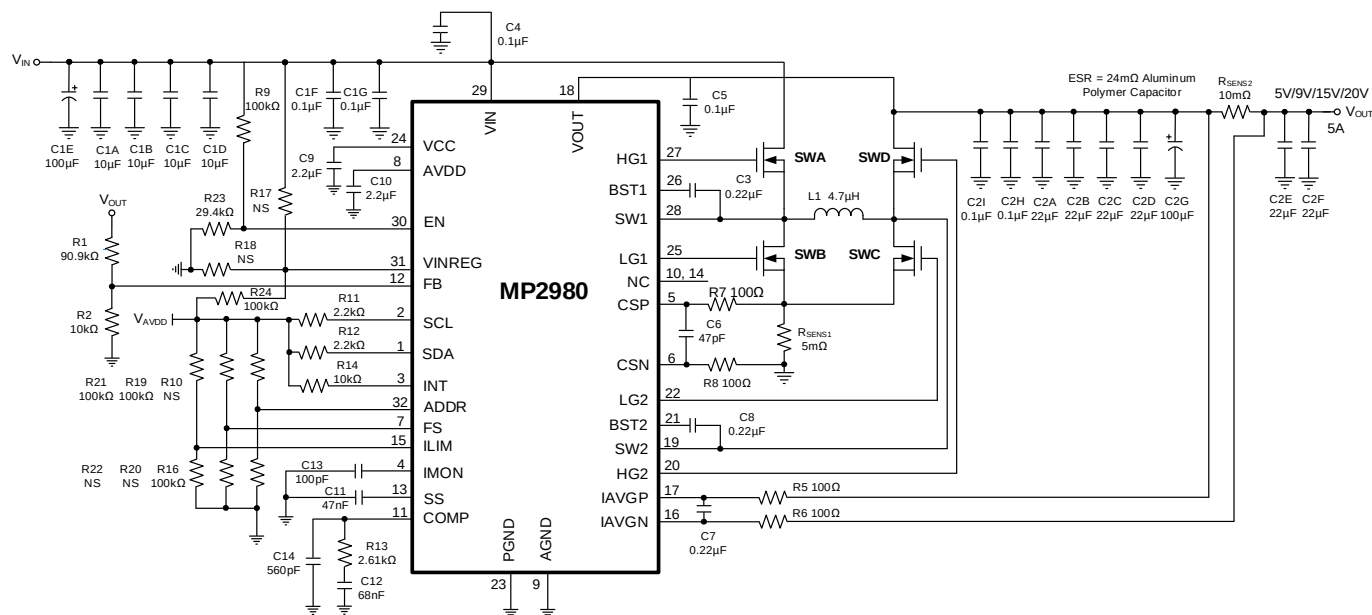


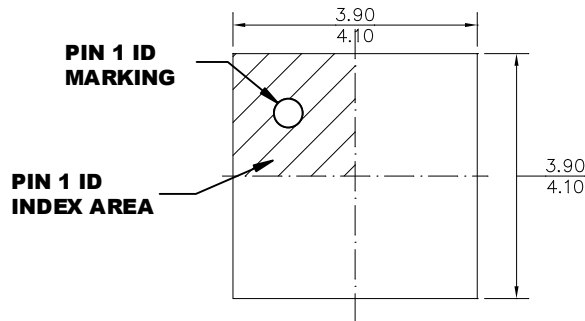
Figure 14: Typical Application Circuit ($V_{IN} = 12V$, $V_{OUT} = 5V/9V/15V/20V$ for 100W)

Note:

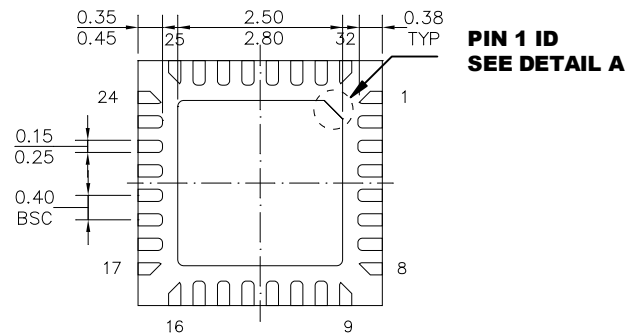
- 13) For USB PD applications, it is recommended to set ADDR equal to AVDD, which turns off the MP2980 by default. Otherwise, set ADDR equal to AGND, which turns on the MP2980 by default (see Table 1 on page 28).

PACKAGE INFORMATION

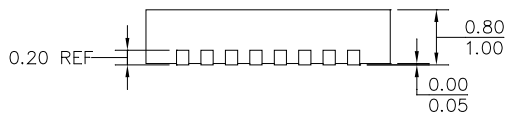
QFN-32 (4mmx4mm)



TOP VIEW

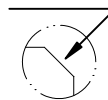


BOTTOM VIEW

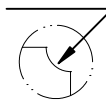


SIDE VIEW

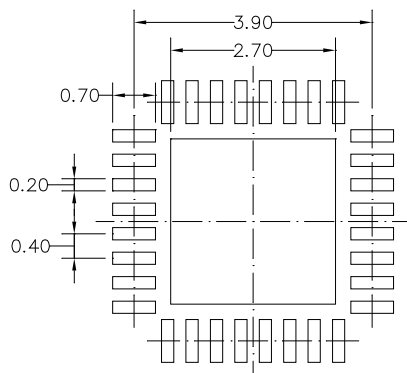
**PIN 1 ID OPTION A
0.30x45° TYP.**



**PIN 1 ID OPTION B
R0.25 TYP.**



DETAIL A

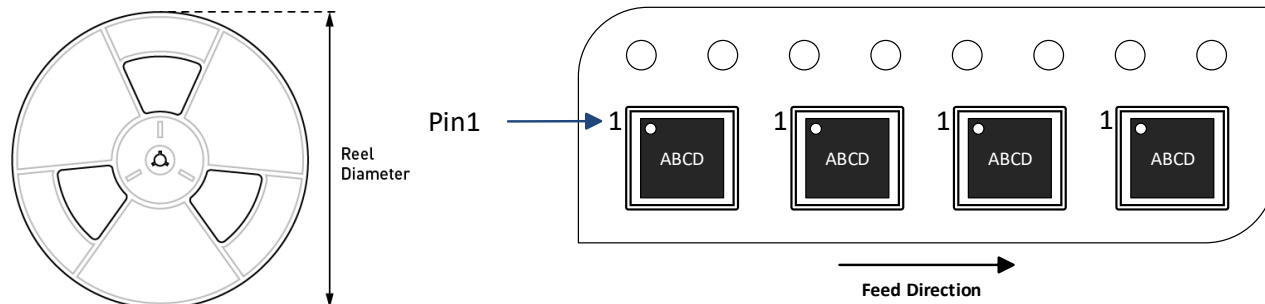


RECOMMENDED LAND PATTERN

NOTE:

- 1) ALL DIMENSIONS ARE IN MILLIMETERS.
- 2) EXPOSED PADDLE SIZE DOES NOT INCLUDE MOLD FLASH.
- 3) LEAD COPLANARITY SHALL BE 0.10 MILLIMETERS MAX.
- 4) JEDEC REFERENCE IS MO-220.
- 5) DRAWING IS NOT TO SCALE.

CARRIER INFORMATION



Part Number	Package Description	Quantity/ Reel	Quantity/ Tube	Quantity/ Tray	Reel Diameter	Carrier Tape Width	Carrier Tape Pitch
MP2980GR-Z	QFN-32 (4mmx4mm)	5000	N/A	N/A	13in	12mm	8mm



REVISION HISTORY

Revision #	Revision Date	Description	Pages Updated
1.0	11/9/2023	Initial Release	-

Notice: The information in this document is subject to change without notice. Please contact MPS for current specifications. Users should warrant and guarantee that third-party Intellectual Property rights are not infringed upon when integrating MPS products into any application. MPS will not assume any legal responsibility for any said applications.