

## 1 FEATURES

- 3.3V single supply voltage
- Bus pin fault protection greater than ±40V
- Bus pin ESD protection greater than ±16KV HBM
- Data rates up to 1Mbps
- Extended common-mode range: -7V to 12V
- High input impedance supports 120 nodes
- LVTTL I/O withstands up to 5V
- Adjustable driver transition time improves radiated performance
- Unpowered nodes do not interfere with the bus
- Low current standby mode, 400µA (typical)
- HMT233: Loopback Mode
- HMT234: Ultra-low current sleep mode
- HMT235: Automatic Baud Loopback Mode
- Thermal Shutdown Protection
- No interference on bus inputs and outputs during power-up and power-down

#### **2 APPLICATIONS**

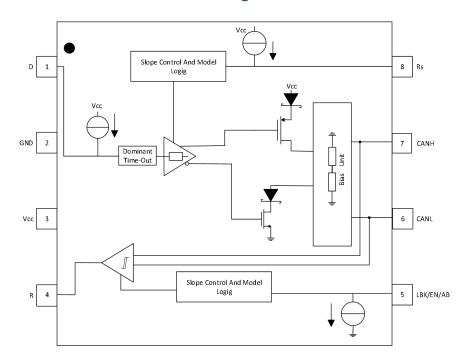
- Industrial Automation, Controls, Sensors and Drive Systems
- Motor and Robot Control
- Building and temperature control (HVAC)
- Backplane communications and control
- CAN open, Device Net, CAN Kingdom, NMEA 2000, SAE J1939 and other CAN bus standard

#### **3 DESCRIPTION**

The HMT233,HMT234,HMT235 are used to applications that utilize the ISO 11898-compliant Controller Area Network (CAN) serial communication physical layer. As a CAN transceiver, each device is used in the differential CAN bus and the CAN controller, each device provides transmit and receive functionality at signaling speeds up to 1Mbps.

Designed for operation in particularly harsh environments, these devices have cross-wire protection, over voltage protection up to ±40V, ground-failure protection, and thermal shutdown protection. These devices can operate over a wide common mode range of -7V to 12V. These transceivers are the interface between the host CAN controller on the microprocessor and the differential CAN bus used in industrial, building automation, transportation, and automotive applications that use differential CAN buses as the applications.

## **Block Diagram**





#### **DESCRIPTION**(continued)

Modes: The RS pin (pin 8) of the HMT233,HMT234 and HMT235 provides three modes of operation: high speed, slope control, and low power standby modes. Directly grounding pin 8 selects the high-speed mode of operation, which allows the driver output transistors to turn on and off as fast as possible with no limit on the rise and fall slopes. The rise and fall slopes can be adjusted by connecting a resistor between the RS pin and ground. The slope will be proportional to the output current of the pin. The device driver has a slew rate of approximately 15V/ $\mu$ s for a resistor value of 10k $\Omega$  and 2.0V/ $\mu$ s for a resistor value of 100k $\Omega$ . See the Feature Description for more information on slope control.If a logic high is applied to the Rs pin, then the HMT233,HMT234,HMT235 enter a low-current standby (listen-only) mode in which the driver is turned off and the receiver remains active. If the local protocol controller needs to send a message to the bus, the device must be returned to high speed mode or ramp control mode via the Rs pin.

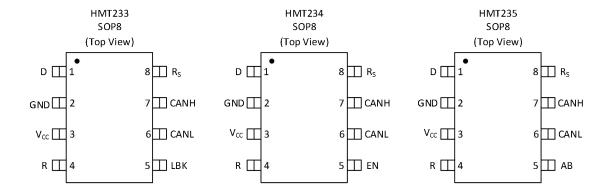
Loopback (HMT233): When the HMT233's loopback (LBK) pin (pin 5) is logic high, it places the bus outputs and bus inputs in a high impedance state. The D to R path inside the device remains active and can be used for driver-to-receiver loopback, enabling the self-diagnostic node function to be performed without disturbing the bus. For more information on the loopback mode, see the <u>Feature Description</u>.

Ultra-Low Current Sleep (HMT234): If a logic low is applied to the EN pin (pin 5), the HMT234 enters an ultra-low current sleep mode in which the driver and receiver circuits are deactivated. The device will remain in this sleep mode until the circuitry is activated by applying a logic high to pin 5.

Auto-Baud Loopback (HMT235): The AB pin (pin 5) of the HMT235 implements a bus listen-only loopback feature that allows the local node controller to synchronize its baud rate with that of the CAN bus. In auto baud mode, the driver's bus output is in a high impedance state while the receiver's bus input remains active. The device has an internal loopback path from the D pin to the R pin to help the controller perform baud rate detection or autobaud functions. See the Feature Description for more information on Auto-Baud mode.



# **4 Pin Configuration and Functions**



Pi	Pin		Pin		Description
Name	No.	1/0	Description		
D	1	I	CAN transmit data input (LOW for dominant and HIGH for recessive bus states), also called TXD, driver input		
GND	2	GND	Ground connection		
V <sub>CC</sub>	3	Supply	Transceiver 3.3V supply		
R	4	0	CAN receive data output (LOW for dominant and HIGH for recessive bus states), also called output		
LBK			HMT233: Loopback mode input pin		
EN	5	ı	HMT234: Enable input pin. Logic high for enabling a normal mode (high speed or slope control) mode. Logic low for sleep mode.		
AB			HMT235: Autobaud loopback mode input pin		
CANL	6	I/O	Low level CAN bus line		
CANH	7	I/O	High level CAN bus line		
Rs	8	I	Mode select pin: strong pulldown to GND = high speed mode, strong pullup to $V_{CC}$ = low power mode, $10K\Omega$ to $100k\Omega$ pulldown to GND = slope control mode		

# **5 Specifications**

# 5.1 Absolute Maximum Ratings(1)(2)

See over operating free-air temperature range unless otherwise noted

Parameter	Description	MIN	MAX	UNIT
	Supply voltage	-0.3	7	V
V <sub>CC</sub>	voltage at any bus terminal (CANH or CANL)	-40	40	V
Vı	Input voltage(D,R <sub>S</sub> ,EN,LBK,AB)	-0.5	7	V
Vo	Output voltage	-0.5	7	V
Io	Receiver output current	-10	10	mA
T <sub>J</sub>	Operating junction temperature		150	°C
T <sub>stg</sub>	Storage temperature		125	

<sup>(1)</sup> Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability

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<sup>(2)</sup> All voltage Values, except differential I/O bus voltages, are with respect to network ground pin.



## 5.2 ESD Ratings

			Value	Unit
V(ESD)	Human body model (HBM)	CANH, CANL and GND	±16000	
Electrostatic	Human body model (HBIVI)	All pins	±4000	V
discharge	Charged-device model (CDM)		±2000	

## **5.3 Recommended Operating Condition**

Parameter	Description	MIN	MAX	UNIT	
.,	Supply voltage			3.6	V
V <sub>CC</sub>	V <sub>CC</sub> voltage at any bus terminal (separately or common mode)		-7	12	V
$V_{IH}$	High-level input voltage	D,EN,AB,LBK	2	5.5	V
$V_{IL}$	Low-level input voltage	D,EN,AB,LBK	0	0.8	V
	Differential input voltage between CANH	and CANL	-6	6	V
$V_{ID}$	Resistance from R <sub>s</sub> to ground	0	100	kΩ	
$V_{I(Rs)}$	Input voltage at R <sub>s</sub> for standby		0.75V <sub>cc</sub>	5.5	V
		Driver	-50		
I <sub>ОН</sub>	High-level output current	Receiver	-10		mA
		Driver		50	
I <sub>OL</sub>	Low-level output current Receiver			10	mA
Tı	Operating junction temperature HMT233,HMT234,HMT235			150	°C
T <sub>A</sub>	Operating free-air temperature <sup>(1)</sup>	HMT233,HMT234,HMT235	-40	125	°C

<sup>(1)</sup> Maximum free-air temperature operation is allowed as long as the device maximum junction temperature is not exceeded.



## **5.4 Electrical Characteristics: Driver**

over operating free-air temperature range (unless otherwise noted)

Parameter	Desc	ription	Test Conditions	MIN	TYP <sup>(1)</sup>	MAX	UNIT
	Bus output	CANH	Data OV Data OV Constitution of Figure 3	2.45		V <sub>CC</sub>	٧
$V_{O(D)}$	voltage (Dominant)	CANL	D at OV, R <sub>s</sub> at OV, See <u>Figure1</u> and <u>Figure 2</u>	0.5		1.0	٧
.,	Bus output	CANH			2.3		.,
Vo	voltage (Dominant)	CANL	D at 3V, R <sub>S</sub> at 0V, See <u>Figure 1</u> and <u>Figure 2</u>		2.3		V
V	Differential	output	D at OV, R <sub>S</sub> at OV, See Figure 1 and Figure 2	1.5	2	3	V
$V_{OD(D)}$	voltage (Do	minant)	D at OV, R <sub>S</sub> at OV, See Figure 2 and Figure 3	1.2	2	3	V
V	Differential	output	D at 3V, R <sub>s</sub> at 0V, See Figure 1 and Figure 2	-120		12	mV
$V_{OD}$	voltage (Re	cessive)	D at 3V, R <sub>s</sub> at 0V, No Load	-0.5		0.05	V
V <sub>OC(pp)</sub>	Peak-to-pea common-m voltage	ak ode output	See Figure 9		1		V
Ιιн	High-level input current	D,EN,LBK,AB	D = 2V or EN = 2V or LBK=2V or AB=2V	-10	-2.5	10	μΑ
I <sub>IL</sub>	Low-level input current	D,EN,LBK,AB	D = 0.8V or EN = 0.8V or LBK=0.8V or AB=0.8V	-15	-6.0	15	μΑ
			VCANH = -7V, CANL Open, See Figure 14	-250			
	Short-circui	t output	VCANH = 12V, CANL Open, See Figure 14			1	^
l <sub>os</sub>	current		VCANL = -7V, CANH Open, See Figure 14	-1			mA
			VCANL = 12V, CANH Open, See Figure 14			250	
I <sub>IRs(s)</sub>	R <sub>s</sub> input cur standby	rent for	R <sub>S</sub> at 0.75V <sub>CC</sub>	-10			μΑ
		Sleep	EN at OV, D at V <sub>CC</sub> , R <sub>S</sub> at OV or V <sub>CC</sub>		0.2	2	
	Supply	Standby	$R_S$ at $V_{CC},D$ at $V_{CC},AB$ at OV,LBK at OV,EN at $V_{CC}$		400	600	μΑ
Icc	current	Dominant	D at OV, No Load, AB at OV,LBK at OV,Rs at OV, EN at $V_{\text{CC}}$		1	2	
Current		Recessive	D at $V_{\text{CC}}$ , No Load, AB at OV,LBK at OV,Rs at OV, EN at $V_{\text{CC}}$		1	2	mA

<sup>(1)</sup> All typical Values are at 25°C and with a 3.3V supply



## **5.5 Electrical Characteristics: Receiver**

over operating free-air temperature range (unless otherwise noted)

Parameter	Descripti	on	Test Condition	ons	MIN	TYP <sup>(1)</sup>	MAX	UNIT	
V <sub>IT+</sub>	Positive-going in threshold voltage					750	900		
$V_{\text{IT-}}$	Negative-going in threshold voltage		AB at OV,LBK at OV,EN a <u>Table 1</u>	at V <sub>CC</sub> , See	500	650		mV	
$V_{hys}$	Hysteresis voltag –V <sub>IT</sub> –)	ge (V <sub>IT+</sub>				100			
$V_{OH}$	High-level outpu	t voltage	I <sub>O</sub> = -4mA, See <u>Figure 6</u>	<u>5</u>	2.4			V	
$V_{OL}$	Low-level output	t voltage	I <sub>O</sub> = 4mA, See <u>Figure 6</u>				0.4	V	
			CANH or CANL at 12V		150		500		
	Bus input current		CANH or CANL at 12V,V <sub>CC</sub> at 0V	Other bus pin at 0V, D	200		600		
l <sub>l</sub>			CANH or CANL at –7V	at 3V, EN at -610		-150	μΑ		
			CANH or CANL at -7V,V <sub>CC</sub> at 0V	V <sub>cc</sub>	-450		-130		
R <sub>ID</sub>	Differential input resistance				40	70	100		
R <sub>IN</sub>	Input resistance (CANH or CANL) to ground		D at 3V,EN at V <sub>CC</sub>		20	35	50	kΩ	
		Sleep	EN at OV, D at V <sub>CC</sub> , R <sub>S</sub> at	: 0V or V <sub>CC</sub>		0.2	2		
		Standby	$R_S$ at $V_{CC}$ , D at $V_{CC}$ , AB at $OV$ , EN at $V_{CC}$	OV,LBK at		400	600	μΑ	
I <sub>cc</sub>	Supply current	Dominant	D at OV, No Load, AB at OV, Rs at OV, EN at Vcc	: OV,LBK at		1	2	nn A	
	Recessive		D at V <sub>CC</sub> , No Load, AB a OV,R <sub>S</sub> at OV, EN at V <sub>CC</sub>	t OV,LBK at		1	2	mA	

<sup>(1)</sup> All typical Values are at 25°C and with a 3.3V supply.



## **5.6 Switching Characteristics: Driver**

over operating free-air temperature range (unless otherwise noted)

Parameter	Description	Test Conditions	MIN	TYP <sup>(1)</sup>	MAX	UNIT
		R <sub>S</sub> at OV, See <u>Figure 4</u>		55	85	
$t_{PLH}$	Propagation delay time, low-to-high-level output	$R_S$ with $10K\Omega$ to ground, See Figure 4		70	125	ns
	low to high level output	$R_S$ with 100K $\Omega$ to ground, See Figure 4		500	870	
		R <sub>S</sub> at OV, See <u>Figure 4</u>		80	120	
$t_{PHL}$	Propagation delay time, high-to-low-level output	$R_S$ with $10k\Omega$ to ground, See Figure 4		130	180	ns
	g to lost lose output	$R_S$ with $100k\Omega$ to ground, See Figure 4		870	1200	
		R <sub>S</sub> at OV, See <u>Figure 4</u>		35		
$t_{sk(p)}$	Pulse skew ( t <sub>PHL</sub> – t <sub>PLH</sub>  )	$R_S$ with $10k\Omega$ to ground, See Figure 4		60		ns
		$R_S$ with $100k\Omega$ to ground, See Figure 4		370		
t <sub>r</sub>	Differential output signal rise time		20		70	
t <sub>f</sub>	Differential output signal fall time	R <sub>S</sub> at OV, See Figure 4	20		70	ns
<b>t</b> r	Differential output signal rise time		30		135	
t <sub>f</sub>	Differential output signal fall time	$R_S$ with $10k\Omega$ to ground, See Figure 4	30		135	ns
t <sub>r</sub>	Differential output signal rise time		350		1400	
t <sub>f</sub>	Differential output signal fall time	$R_S$ with 100k $\Omega$ to ground, See <u>Figure 4</u>	350		1400	ns
t <sub>en(s)</sub>	Enable time from standby to dominant	See Figure 7 and Figure 9		0.6	1.5	
t <sub>en(z)</sub>	Enable time frome sleep to dominant	See Figure 7 and Figure 8		1	5	μs

<sup>(1)</sup> All typical Values are at 25°C and with a 3.3V supply.

## **5.7 Switching Characteristics: Receiver**

over operating free-air temperature range (unless otherwise noted)

Parameter	Description	Test Conditions	MIN	TYP <sup>(1)</sup>	MAX	UNIT
t <sub>PLH</sub>	Propagation delay time, low-to-high-level output			35	60	
t <sub>PHL</sub>	Propagation delay time, high-to-low-level output			35	60	
t <sub>sk(p)</sub>	Pulse skew ( t <sub>PHL</sub> - t <sub>PLH</sub>  )	See <u>Figure 6</u>		7		ns
t <sub>r</sub>	Output signal rise time			3	5	
t <sub>f</sub>	Output signal fall time			3	5	

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<sup>(1)</sup> All typical Values are at 25°C and with a 3.3V supply.



# **5.8 Switching Characteristics: Device**

over operating free-air temperature range (unless otherwise noted)

Parameter		Test Conditions	MIN	TYP <sup>(1)</sup>	MAX	UNIT	
t <sub>(LBK)</sub>	Loopback delay, driver input to receiver output	HMT233	See <u>Figure 11</u>		7.5	12	
t <sub>(AB1)</sub>	Loopback delay, driver		See Figure 12		10	20	ns
t <sub>(AB2)</sub>			See <u>Figure 13</u>		35	60	
			R <sub>S</sub> at OV, See <u>Figure 10</u>		90	135	
t <sub>(loop1)</sub>	Total loop delay, driver inpu		$R_S$ with $10k\Omega$ to ground, See Figure $\underline{10}$		105	190	ns
	output, recessive to dominant		$R_{S}$ with 100K $\Omega$ to ground, See Figure $\underline{10}$		535	1000	
			R <sub>S</sub> at OV, See Figure 10		100	135	
t <sub>(loop2)</sub>	Total loop delay, driver input to receiver $t_{(loop2)}$		$R_S$ with $10K\Omega$ to ground, See Figure $10$		125	190	ns
	output, dominant to recessi	ve	$R_S$ with 100KΩ to ground, See Figure $\underline{10}$		535	1000	

<sup>(1)</sup> All typical Values are at 25°C and with a 3.3V supply.



## **6 Parameter Measurement Information**

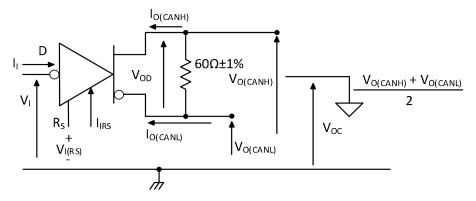
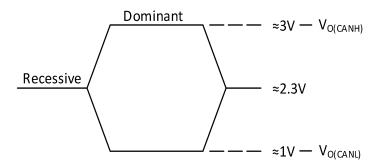


Figure 1 Driver Voltage, Current, and Test Definition



**Figure 2 Bus Logic State Voltage Definitions** 

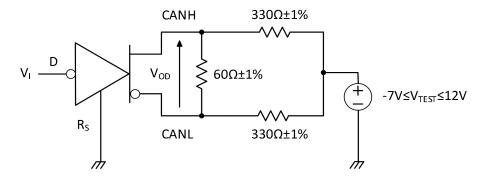
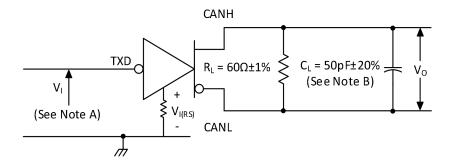


Figure 3 Driver VoD

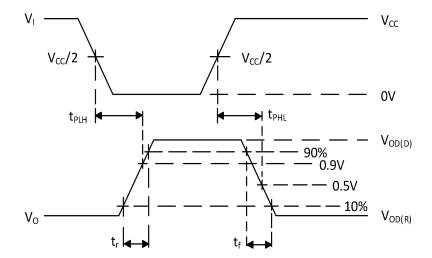


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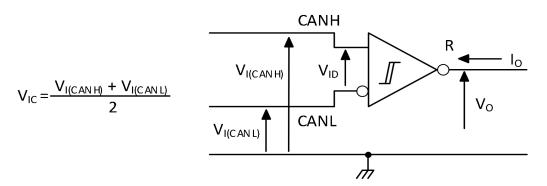




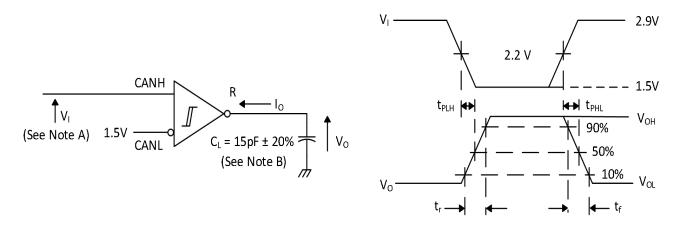
A. The input pulse is supplied by a generator having the following characteristics: Pulse repetition rate (PRR)  $\leq$  125kHz, 50% duty cycle,  $t_r \leq$  6ns,  $t_f \leq$ 

B. CL includes fixture and instrumentation capacitance.

**Figure 4 Driver Test Circuit and Voltage Waveforms** 



**Figure 5 Receiver Voltage and Current Definitions** 



A.The input pulse is supplied by a generator having the following characteristics: Pulse repetition rate (PRR)  $\leq$  125 kHz, 50% duty cycle,  $t_r \leq$  6ns,  $t_f \leq$ 

B.CL includes fixture and instrumentation capacitance.

**Figure 6 Receiver Test Circuit and Voltage Waveforms** 

Χ

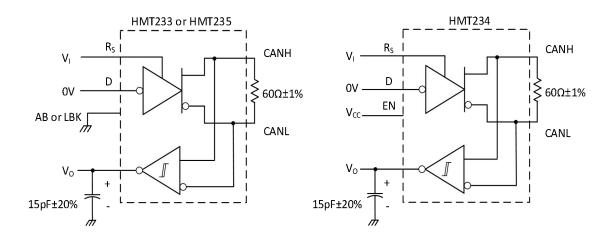


Open

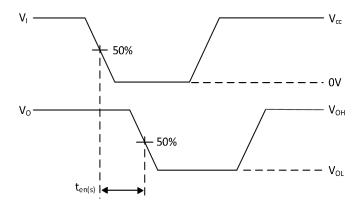
INF	INPUT		ITPUT	MEASURED
VCANH	VCANL		R	[VID]
-6.1V	-7V	L		900mV
12V	11.1V	L	7	900mV
-1V	-7V	L	VOL	6V
12V	6V	L		6V
-6.5V	-7V	Н		500mV
12V	11.5V	Н		500mV
-7V	-1V	Н	VOH	6V
6V	12V	Н		6V

Н

**Table 1 Differential Input Voltage Threshold Test** 



Open



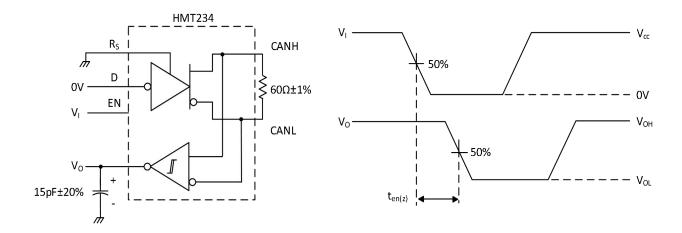
NOTE: All VI input pulses are supplied by a generator having the following characteristics:  $t_r$  or  $t_f \le 6$ ns, pulse repetition rate (PRR) = 125kHz, 50% duty cycle.

Figure 7 T<sub>en(s)</sub> Test Circuit and Voltage Waveforms

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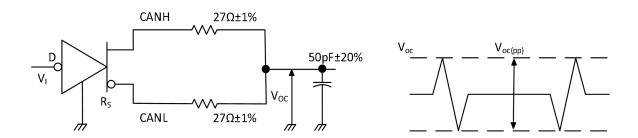
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NOTE: All VI input pulses are supplied by a generator having the following characteristics:  $t_r$  or  $t_f \le 6$ ns, pulse repetition rate (PRR) = 50kHz, 50% duty cycle.

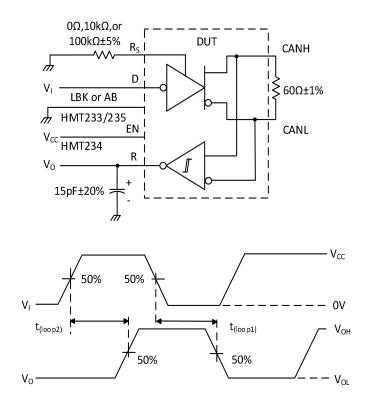
Figure 8 Ten(z) Test Circuit and Voltage Waveforms



NOTE: All VI input pulses are supplied by a generator having the following characteristics:  $t_r$  or  $t_f \le 6$ ns, pulse repetition rate (PRR) = 125 kHz, 50% duty cycle.

Figure 9  $V_{\text{OC(pp)}}$  Test Circuit and Voltage Waveforms



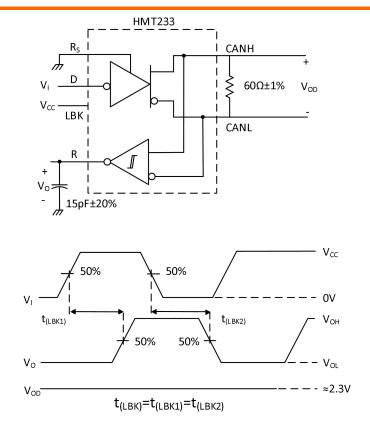


NOTE: All VI input pulses are supplied by a generator having the following characteristics:  $t_r$  or  $t_f \le 6$ ns, pulse repetition rate (PRR) = 125 kHz, 50% duty cycle.

Figure 10 T<sub>(loop)</sub> Test Circuit and Voltage Waveforms

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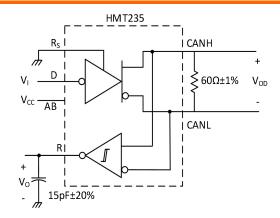


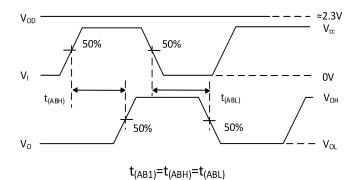


NOTE: All VI input pulses are supplied by a generator having the following characteristics: tr or tf  $\leq$  6ns, pulse repetition rate (PRR) = 125 kHz, 50% duty cycle.

Figure 11 T<sub>(LBK)</sub> Test Circuit and Voltage Waveforms

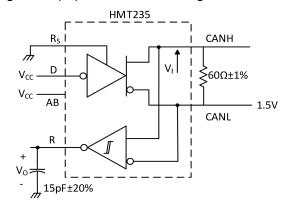


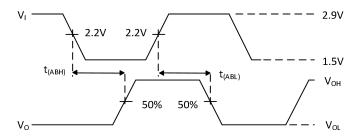




NOTE: All VI input pulses are supplied by a generator having the following characteristics: tr or tf  $\leq$  6ns, pulse repetition rate (PRR) = 125 kHz, 50% duty cycle.

Figure 12 T<sub>(AB1)</sub> Test Circuit and Voltage Waveforms





 $t_{(AB2)}=t_{(ABH)}=t_{(ABL)}$ 

NOTE: All VI input pulses are supplied by a generator having the following characteristics:  $t_r$  or  $t_f \le 6$ ns, pulse repetition rate (PRR) = 125 kHz, 50% duty cycle.

Figure 13 T<sub>(AB2)</sub> Test Circuit and Voltage Waveforms

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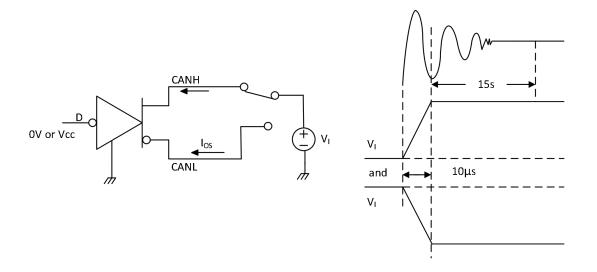
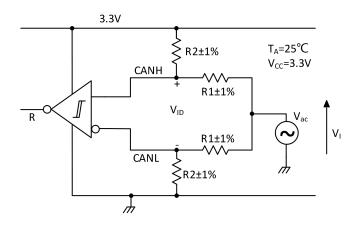


Figure 14 Ios Test Circuit and Waveforms



The R Output State Does Not Change During Application of the Input Waveform.

VID	R1	R2
500mV	50	280
900mV	50	130



NOTE: All input pulses are supplied by a generator with  $f \le 1.5 MHz$ 

Figure 15 Common-Mode Voltage Rejection

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## **7 Detailed Description**

## 7.1 Overview

This family of CAN transceivers is compatible with the ISO11898-2 High-Speed CAN (controller area network) physical layer standard. They are designed to interface between the differential bus lines in CAN and the CAN protocol controller at data rates up to 1Mpbs.

## 7.2 Functional Block Diagrams

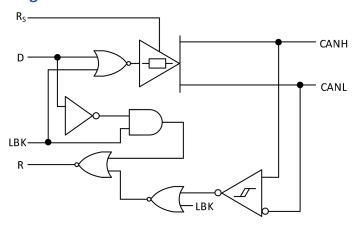


Figure 16. HMT233 Functional Block Diagram

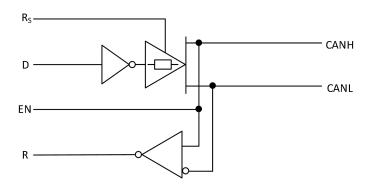


Figure 17. HMT234 Functional Block Diagram

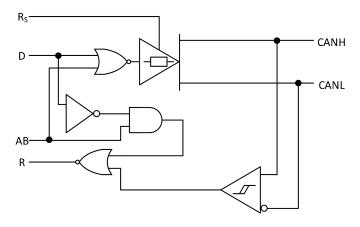


Figure 18. HMT235 Functional Block Diagram



## 7.3 Feature Description

#### 7.3.1 Diagnostic Loopback (HMT233)

The diagnostic loopback or internal loopback function of the HMT233 is enabled with a high-level input on pin 5, LBK. This mode disables the driver output while keeping the bus pins biased to the recessive state. This mode also redirects the D data input (transmit data) through logic to the received data output pin), thus creating an internal loopback of the transmit to receive data path. This mimics the loopback that occurs normally with a CAN transceiver because the receiver loops back the driven output to the R (receive data) pin. This mode allows the host protocol controller to input and read back a bit sequence or CAN messages to perform diagnostic routines without disturbing the CAN bus. A typical CAN bus application is displayed in Figure 23. If the LBK pin is not used it may be tied to ground (GND). However, it is pulled low internally (defaults to a low-level input) and may be left open if not in use.

#### 7.3.2Autobaud Loopback (HMT235)

The autobaud loopback mode of the HMT235 is enabled by placing a high level input on pin 5, AB. In autobaud mode, the driver output is disabled, thus blocking the D pin to bus path and the bus transmit function of the transceiver. The bus pins remain biased to recessive. The receiver to R pin path or the bus receive function of the device remains operational, allowing bus activity to be monitored. In addition, the autobaud mode adds an internal logic loopback path from the D pin to R pin so the local node may transmit to itself in sync with bus traffic while not disturbing messages on the bus. Thus if the local node 's CAN controller generates an error frame, it is not transmitted to the bus, but is detected only by the local CAN controller. This is especially helpful to determine if the local node is set to the same baud rate as the network, and if not adjust it to the network baud rate (autobaud detection).

Autobaud detection is best suited to applications that have a known selection of baud rates. For example, a popular industrial application has optional settings of 125kbps, 250kbps, or 500kbps. Once the HMT235 is placed into autobaud loopback mode the application software could assume the first baud rate of 125kbps. It then waits for a message to be transmitted by another node on the bus. If the wrong baud rate has been selected, an error message is generated by the local CAN controller because the sample times will not be at the correct time. However, because the bus-transmit function of the device has been disabled, no other nodes receive the error frame generated by this node's local CAN controller.

The application would then make use of the status register indications of the local CAN controller for message received and error warning status to determine if the set baud rate is correct or not. The warning status indicates that the CAN controller error counters have been incremented. A message received status indicates that a good message has been received. If an error is generated, the application would then set the CAN controller with the next possibly valid baud rate, and wait to receive another message. This pattern is repeated until an error free message has been received, thus the correct baud rate has been selected. At this point the application would place the HMT235 in a normal transmitting mode by setting pin 5 to a low-level, thus enabling bus-transmit and bus-receive functions to normal operating states for the transceiver.

If the AB pin is not used it may be tied to ground (GND). However, it is pulled low internally (defaults to a low-level input) and may be left open if not in use.

#### 7.3.3 Slope Control

The rise and fall slope of the HMT233,HMT234,HMT235 driver output can be adjusted by connecting a resistor from the Rs (pin 8) to ground (GND), or to a low-level input voltage as shown in <u>Figure 19</u>.

The slope of the driver output signal is proportional to the pin's output current. This slope control is implemented with an external resistor Value of  $10K\Omega$  to achieve a ~15V/µs slew rate, and up to  $100K\Omega$  to achieve a ~2.0V/µs slew rate . A typical slew rate Verses pulldown resistance graph is shown in Figure 20. Typical driver output wave forms with slope control are displayed in Figure 25.

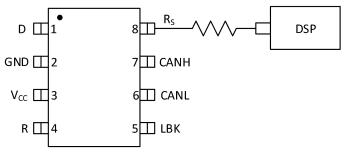


Figure 19. Slope Control/Standby Connection to a DSP



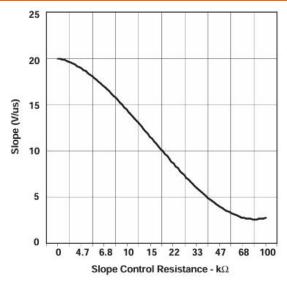


Figure 20. HVD233 Driver Output Signal Slope vs Slope Control Resistance Value

#### **7.3.4 Standby**

If a high-level input ( $> 0.75V_{CC}$ ) is applied to  $R_S$  (pin 8), the circuit enters a low-current, listen only standby mode during which the driver is switched off and the receiver remains active. If using this mode to save system power while waiting for bus traffic, the local controller can monitor the R output pin for a falling edge which indicates that a dominant signal was driven onto the CAN bus. The local controller can then drive the  $R_S$  pin low to return to slope control mode or high-speed mode.

#### 7.3.5 Thermal Shutdown

If the junction temperature of the device exceeds the thermal shut down threshold the device turns off the CAN driver circuits thus blocking the D pin to bus transmission path. The shutdown condition is cleared when the junction temperature drops below the thermal shutdown temperature of the device. The CAN bus pins are high impedance biased to recessive level during a thermal shutdown, and the receiver to R pin path remains operational.

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# 7.4 Device Functional Modes

## Table 2. Driver (HMT233 or HMT235)

	INPUTS		OUTPUTS			
D	D LBK/AB Rs CANH CANL				BUS STATE	
X	Х	> 0.75 V <sub>CC</sub>	Z	Z	Recessive	
L	L or open	< 0.22.1/	Н	L	Dominant	
H or open	Х	≤ 0.33 V <sub>cc</sub>	Z	Z	Recessive	
Х	Н	≤ 0.33 V <sub>cc</sub>	Z	Z	Recessive	

## Table 3. Receiver (HMT233)

INPUTS				OUTPUT
BUS STATE	VID = V(CANH)-V(CANL)	LBK	D	R
Dominant	VID ≥ 0.9 V	L or open	Х	L
Recessive	VID ≤ 0.5 V or open	L or open	H or open	Н
?	0.5 V < VID <0.9 V	L or open	H or open	?
Х	X		L	L
Х	X	Н	Н	Н

## Table 4. Receiver (HMT235)<sup>(1)</sup>

INPUTS				
BUS STATE	VID = V(CANH)-V(CANL)	AB	D	R
Dominant	VID ≥ 0.9 V	L or open	Х	L
Recessive	VID ≤ 0.5 V or open	L or open	H or open	Н
?	0.5 V < VID <0.9 V	L or open	H or open	?
Dominant	VID ≥ 0.9 V	Н	Х	L
Recessive	VID ≤ 0.5 V or open	Н	Н	Н
Recessive	VID ≤ 0.5 V or open	Н	L	L
?	0.5 V < VID < 0.9 V	Н	L	L

<sup>(1)</sup> H = high level; L = low level; Z = high impedance; X = irrelevant; ? = indeterminate

## Table 5.Driver(HMT234)

INPUTS				OUTPUTS		
D	EN	Rs	CANH	CANL	BUS STATE	
L	Н	≤ 0.33V <sub>CC</sub>	Н	L	Dominant	
Н	X	≤ 0.33V <sub>CC</sub>	Z	Z	Recessive	
Open	X	X	Z	Z	Recessive	
Х	Х	> 0.75V <sub>CC</sub>	Z	Z	Recessive	
Х	L or open	Х	Z	Z	Recessive	



Table	6.Receiver	(HMT234)	(1)
-------	------------	----------	-----

	OUTPUT		
BUS STATE	VID =V(CANH)-V(CANL)	EN	R
Dominant	VID≥ 0.9V	Н	L
Recessive	VID ≤ 0.5V or open	Н	Н
?	0.5V <vid <0.9v<="" td=""><td>Н</td><td>?</td></vid>	Н	?
Х	X	L or open	Н

(1) H = high level; L = low level; Z = high impedance; X = irrelevant; ? = indeterminate

## **8 Application and Implementation**

## **8.1 Application Information**

The CAN bus has two states during powered operation of the device; dominant and recessive. A dominant bus state is when the bus is driven differentially, corresponding to a logic low on the D and R pin. A recessive bus state is when the bus is biased to  $V_{CC}$  / 2 via the high-resistance internal resistors  $R_{IN}$  and  $R_{ID}$  of the receiver, corresponding to a logic high on the D and R pins. See Figure 21 and Figure 22.

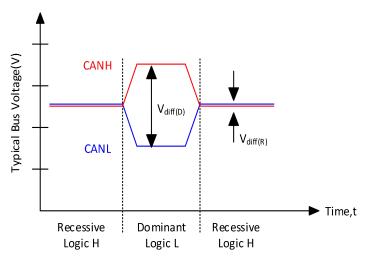


Figure 21. Bus States (Physical Bit Representation)

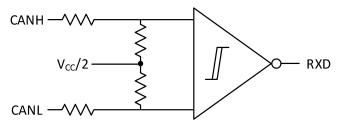


Figure 22. Simplified Recessive Common Mode Bias and Receiver

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These CAN transceivers are typically used in applications with a host microprocessor or FPGA that includes the link layer portion of the CAN protocol. The different nodes on the network are typically connected through the use of a  $120\Omega$  characteristic impedance twisted-pair cable with termination on both ends of the bus.



## 8.2 Typical Application

#### 8.2.1 Design Requirements

#### 8.2.1.1 Bus Loading, Length and Number of Nodes

The ISO 11898 Standard specifies up to a data rate of 1Mbps, maximum CAN bus cable length of 40 m, maximum drop line (stub) length of 0.3 m and a maximum of 30 nodes. However, with careful network design, the system may have longer cables, longer stub lengths, and many more nodes to a bus. Many CAN organizations and standards have scaled the use of CAN for applications outside the original ISO 11898 standard. They have made system level trade-offs for data rate, cable length, and parasitic loading of the bus. Examples of some of these specifications are ARINC825, CAN open, CAN Kingdom, Device Net and NMEA200.

A high number of nodes requires a transceiver with high input impedance and wide common mode range such as the HMT23X CAN family. ISO 11898-2 specifies the driver differential output with a  $60\Omega$  load (two 120  $\Omega$  termination resistors in parallel) and the differential output must be greater than 1.5V. The HMT23x devices are specified to meet the 1.5V requirement with a  $60\Omega$  load, and additionally specified with a differential output voltage minimum of 1.2V across a common mode range of -2V to 7V through a  $330\Omega$  coupling network. This network represents the bus loading of 120 HMT23x transceivers based on their minimum differential input resistance of  $40K\Omega$ . Therefore, the HMT23x supports up to 120 transceivers on a single bus segment with margin to the 1.2V minimum differential input voltage requirement at each node.

For CAN network design, margin must be given for signal loss across the system and cabling, parasitic loadings, network imbalances, ground offsets and signal integrity thus a practical maximum number of nodes may be lower. Bus length may also be extended beyond the original ISO 11898 standard of 40 m by careful system design and data rate tradeoffs. For example, CAN open network design guidelines allow the network to be up to 1 km with changes in the termination resistance, cabling, less than 64 nodes and significantly lowered data rate.

This flexibility in CAN network design is one of the key strengths of the Various extensions and additional standards that have been built on the original ISO 11898 CAN standard.

## 8.2.1.2 CAN Termination

The ISO 11898 standard specifies the interconnect to be a twisted-pair cable (shielded or unshielded) with  $120\Omega$  characteristic impedance ( $Z_0$ ). Resistors equal to the characteristic impedance of the line should be used to terminate both ends of the cable to prevent signal reflections. Unterminated drop lines (stubs) connecting nodes to the bus should be kept as short as possible to minimize signal reflections. The termination may be on the cable or in a node, but if nodes may be removed from the bus the termination must be carefully placed so that it is not removed from the bus.

#### 8.2.2 Detailed Design Procedure

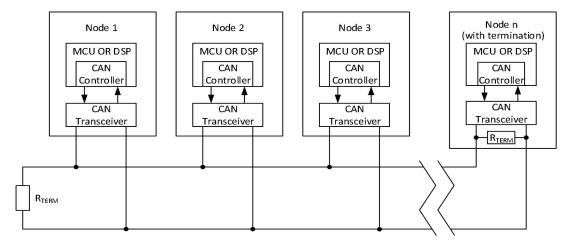


Figure 23. Typical CAN Bus



Termination is typically a  $120\Omega$  resistor at each end of the bus. If filtering and stabilization of the common mode voltage of the bus is desired, then split termination may be used (see Figure 24). Split termination uses two  $60\Omega$  resistors with a capacitor in the middle of these resistors to ground. Split termination improves the electromagnetic emissions behavior of the network by eliminating fluctuations in the bus common mode voltages at the start and end of message transmissions.

Care should be taken in the power ratings of the termination resistors used. Typically the worst case condition would be if the system power supply was shorted across the termination resistance to ground. In most cases the current flow through the resistor in this condition would be much higher than the transceiver's current limit.

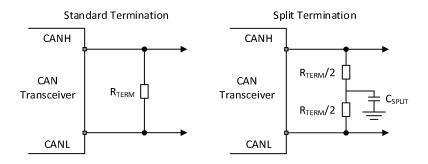


Figure 24. CAN Bus Termination Concepts

#### 8.2.3 Application Curve

Figure 25 shows 3 typical output waveforms for the HMT233 device with three different connections made to the  $R_S$  pin. The top waveform show the typical differential signal when transitioning from a recessive level to a dominant level on the CAN bus with  $R_S$  tied to GND through a  $0\Omega$  resistor. The second waveform shows the same signal for the condition with a  $10k\Omega$  resistor tied from  $R_S$  to ground. The bottom waveform shows the typical differential signal for the case where a  $100k\Omega$  resistor is tied from the  $R_S$  pin to ground.

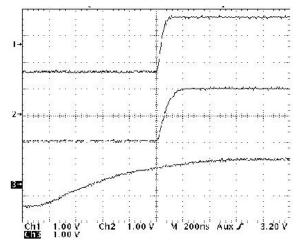


Figure 25. Typical HMT233 Output Waveforms With Different Slope Control Resistor Values

## 8.3 System Example

#### 8.3.1 ISO 11898 Compliance of HMT23x Family of 3.3V CAN Transceivers

#### 8.3.1.1 Introduction

Many users Value the low power consumption of operating their CAN transceivers from a 3.3V supply. However, some are concerned about the interoperability with 5V supplied transceivers on the same bus. This report analyzes this situation to address those concerns.

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#### 8.3.1.2 Differential Signal

CAN is a differential bus where complementary signals are sent over two wires and the voltage difference between the two wires defines the logical state of the bus. The differential CAN receiver monitors this voltage difference and outputs the bus state with a single ended logic level output signal.

The CAN driver creates the differential voltage between CANH and CANL in the dominant state. The dominant differential output of the HMT23x is greater than 1.5V and less than 3V across a 60 ohm load as defined by the ISO 11898 standard. These are the same limiting Values for 5V supplied CAN transceivers. The bus termination resistors drive the recessive bus state and not the CAN driver. A CAN receiver is required to output a recessive state when less than 500mV of differential voltage exists on the bus, and a dominant state when more than 900mV of differential voltage exists on the bus. A CAN receiver must do this with common-mode input voltages from -2V to 7V. The HMT23x family receivers meet these same input specifications as 5V supplied receivers.

#### 8.3.1.3 Common-Mode Signal

A common-mode signal is an average voltage of the two signal wires that the differential receiver rejects. The common-mode signal comes from the CAN driver, ground noise, and coupled bus noise. Since the bias voltage of the recessive state of the device is dependent on  $V_{CC}$ , any noise present or Variation of  $V_{CC}$  will have an effect on this bias voltage seen by the bus. The HMT23x family has the recessive bias voltage set higher than  $0.5*V_{CC}$  to comply with the ISO 11898-2 CAN standard. The caveat to this is that the common mode voltage will drop by a couple hundred millivolts when driving a dominant bit on the bus. This means that there is a common mode shift between the dominant bit and recessive bit states of the device. While this is not ideal, this small Variation in the driver common-mode output is rejected by differential receivers and does not effect data, signal noise margins or error rates.

#### 8.3.1.4 Interoperability of 3.3V CAN in 5V CAN Systems

The 3.3V supplied HMT23x family of CAN transceivers are fully compatible with 5V CAN transceivers. The differential output voltage is the same, the recessive common mode output bias is the same, and the receivers have the same input specifications. The only slight difference is in the dominant common mode output voltage which is a couple hundred millivolts lower for 3.3V CAN transceiver than 5V supplied transceiver.

To help ensure the widest interoperability possible, the HMT23x family has successfully passed the internationally recognized GIFT/ICT conformance and interoperability testing for CAN transceivers. Electrical interoperability does not always assure interchangeability however. Most implementers of CAN buses recognize that ISO 11898 does not sufficiently specify the electrical layer and that strict standard compliance alone does not ensure full interchangeability. This comes only with thorough equipment testing.

## **9 Power Supply Recommendations**

To ensure reliable operation at all data rates and supply voltages, each supply should be decoupled with a 100nF ceramic capacitor located as close to the V<sub>CC</sub> supply pins as possible.



## 10 Layout

## **10.1 Layout Guidelines**

In order for the PCB design to be successful, start with design of the protection and filtering circuitry. Because ESD and EFT transients have a wide frequency bandwidth from approximately 3MHz to 3GHz, high frequency layout techniques must be applied during PCB design. On chip IEC ESD protection is good for laboratory and portable equipment but is usually not sufficient for EFT and surge transients occurring in industrial environments. Therefore robust and reliable bus node design requires the use of external transient protection devices at the bus connectors. Placement at the connector also prevents these harsh transient events from propagating further into the PCB and system. Use  $V_{CC}$  and ground planes to provide low inductance.

Design the bus protection components in the direction of the signal path. Do not force the transient current to divert from the signal path to reach the protection device.

An example placement of the Transient voltage Suppression (TVS) device indicated as D1 (either bi-directional diode or Varistor solution) and bus filter capacitors C5 and C7 are shown in <u>Figure 26</u>.

The bus transient protection and filtering components should be placed as close to the bus connector, J1, as possible. This prevents transients, ESD and noise from penetrating onto the board and disturbing other devices.

Bus termination: Figure 26 shows split termination. This is where the termination is split into two resistors, R5 and R6, with the center or split tap of the termination connected to ground Via capacitor C6. Split termination provides common mode filtering for the bus. When termination is placed on the board instead of directly on the bus, care must be taken to ensure the terminating node is not removed from the bus as this will cause signal integrity issues of the bus is not properly terminated on both ends. See the application section for information on power ratings needed for the termination resistor(s).

Bypass and bulk capacitors should be placed as close as possible to the supply pins of transceiver, examples C2, C3  $(V_{CC})$ .

Use at least two Vias for  $V_{CC}$  and ground connections of bypass capacitors and protection devices to minimize trace and Via inductance.

To limit current of digital lines, serial resistors may be used. Examples are R1, R2, R3 and R4.

To filter noise on the digital IO lines, a capacitor may be used close to the input side of the IO as shown by C1 and C4. Since the internal pullup and pulldown biasing of the device is weak for floating pins, an external  $1k\Omega$  to  $10k\Omega$  pullup or pulldown resistor should be used to bias the state of the pin more strongly against noise during transient events. Pin 1: If an open drain host processor is used to drive the D pin of the device an external pull-up resistor between  $1k\Omega$  and  $10k\Omega$  and  $V_{CC}$  should be used to drive the recessive input state of the device.

Pin 8: is shown assuming the mode pin, R<sub>s</sub>, will be used. If the device will only be used in normal mode or slope control mode, R3 is not needed and the pads of C4 could be used for the pulldown resistor to GND.

#### 10.2 Layout Example

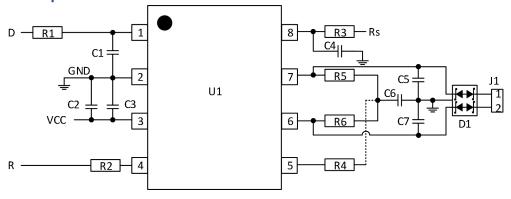
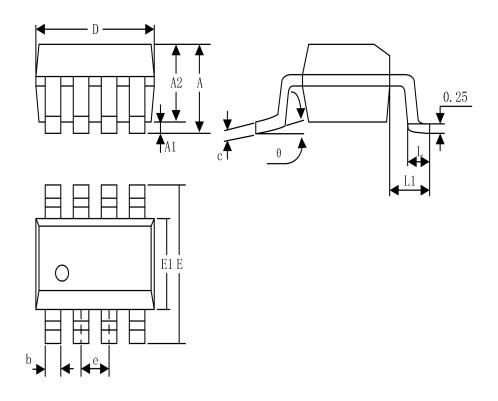


Figure 26. Layout Example Schematic



# PACKAGING DIMENSION SOP8-L



SYMBOLS	MILLIMETER				
	MIN	NOM	MAX		
A	1.5	-	1.7		
A1	0.1	-	0.25		
A2	1.3	1.4	1.5		
b	0.33	0.4	0.47		
С	0.2	-	0.25		
D	4.7	4.9	5.1		
E	5.9	6	6.1		
E1	3.8	3.9	4		
e	1.27(BSC)				
L	0.55	0.6	0.75		
L1	1.05(BSC)				
θ	0°	4°	8°		



# **Order Information**

Order number	Package	Marking information	Operation Temperature Range	MSL Grade	Ship, Quantity	Green
HMT233T	SOP8-L	HMT233T	-40 to 125°C	3	T&R, 2500	Rohs
HMT234T	SOP8-L	HMT234T	-40 to 125°C	3	T&R, 2500	Rohs
HMT235T	SOP8-L	HMT235T	-40 to 125°C	3	T&R, 2500	Rohs